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**NAGBR NAGB8 NAQB , H1N NBH NUJD**

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(54) Abstract Title

**Position detector constructed from conductive fabric**

(57) A position detector incorporates regions 1501-7 having first and second planes of conductive fabric, wherein a mechanical interaction brings the planes of at least one of the regions closer together. The fabric may be woven, knitted or non-woven eg felt. Preferably one of the planes is unique to a region and the other is shared by some or all of the regions. A potential difference applied across at least one of the planes can be used to determine the position of the mechanical interaction. Electrical signals can be derived independently from the regions by Time Division Multiplexing TMD (Fig. 3) via a microcontroller (201, Fig. 2) operated circuit (121, Fig. 2). At least one of the planes may consist of first and second portions (1206, 1205, Figs. 12A, 12B), the first portion having a higher resistance and being more flexible to allow complex curvature (Fig. 12B). Plates (1208, Figs. 12A, 12B) provide additional rigidity to the second portion. A second electrical property eg current or resistance can be used to identify additional properties of the mechanical interaction eg applied force, area of contact or orientation of an object.

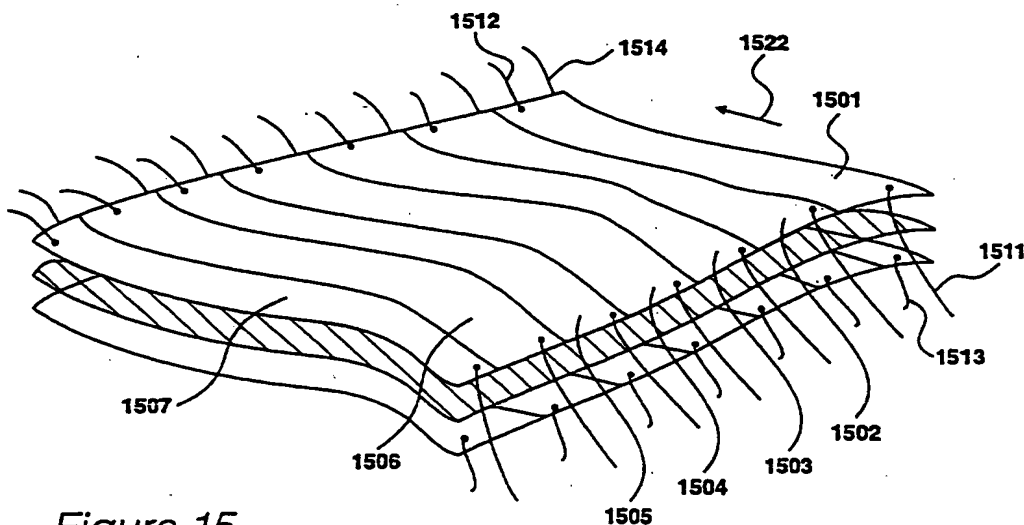


Figure 15

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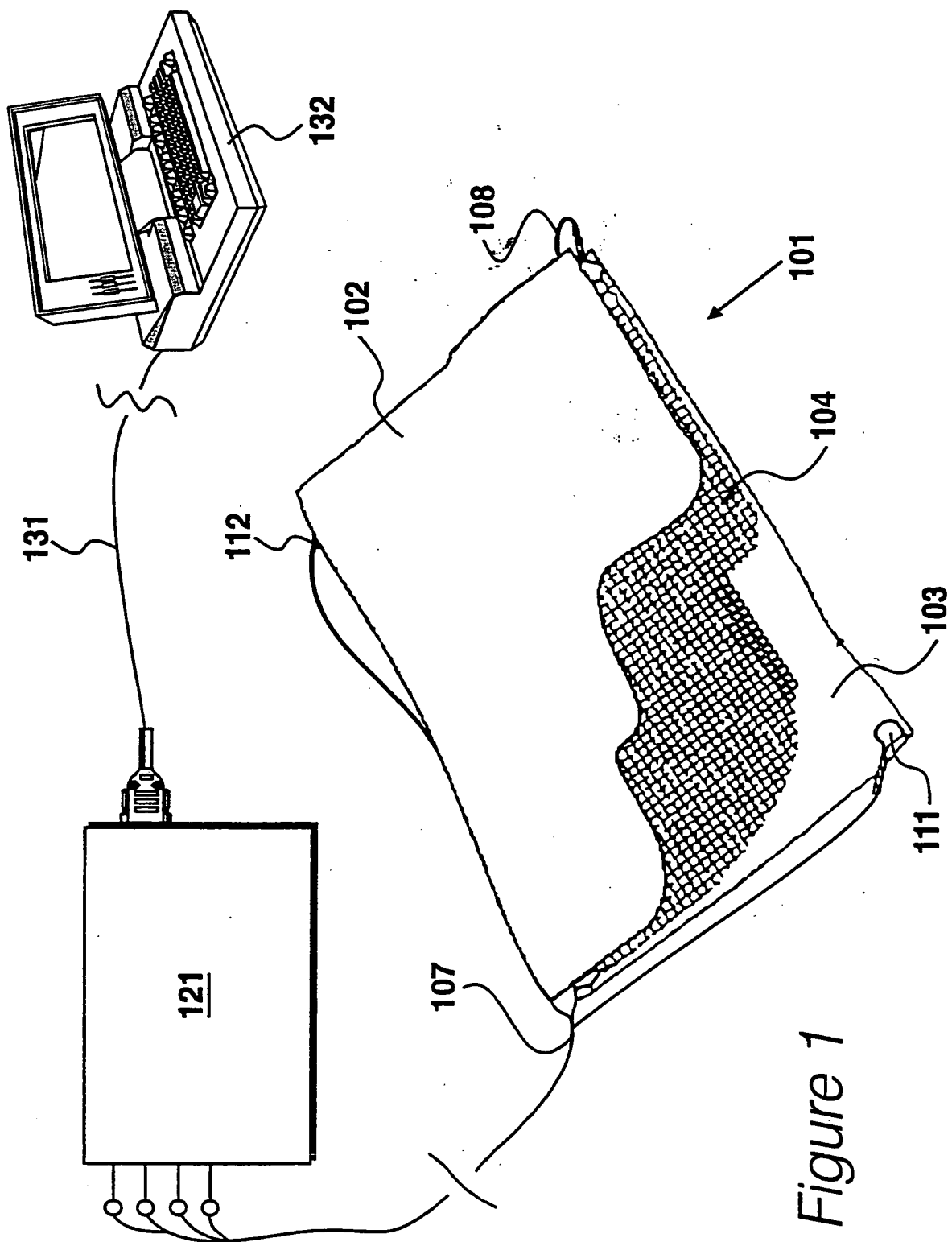


Figure 1

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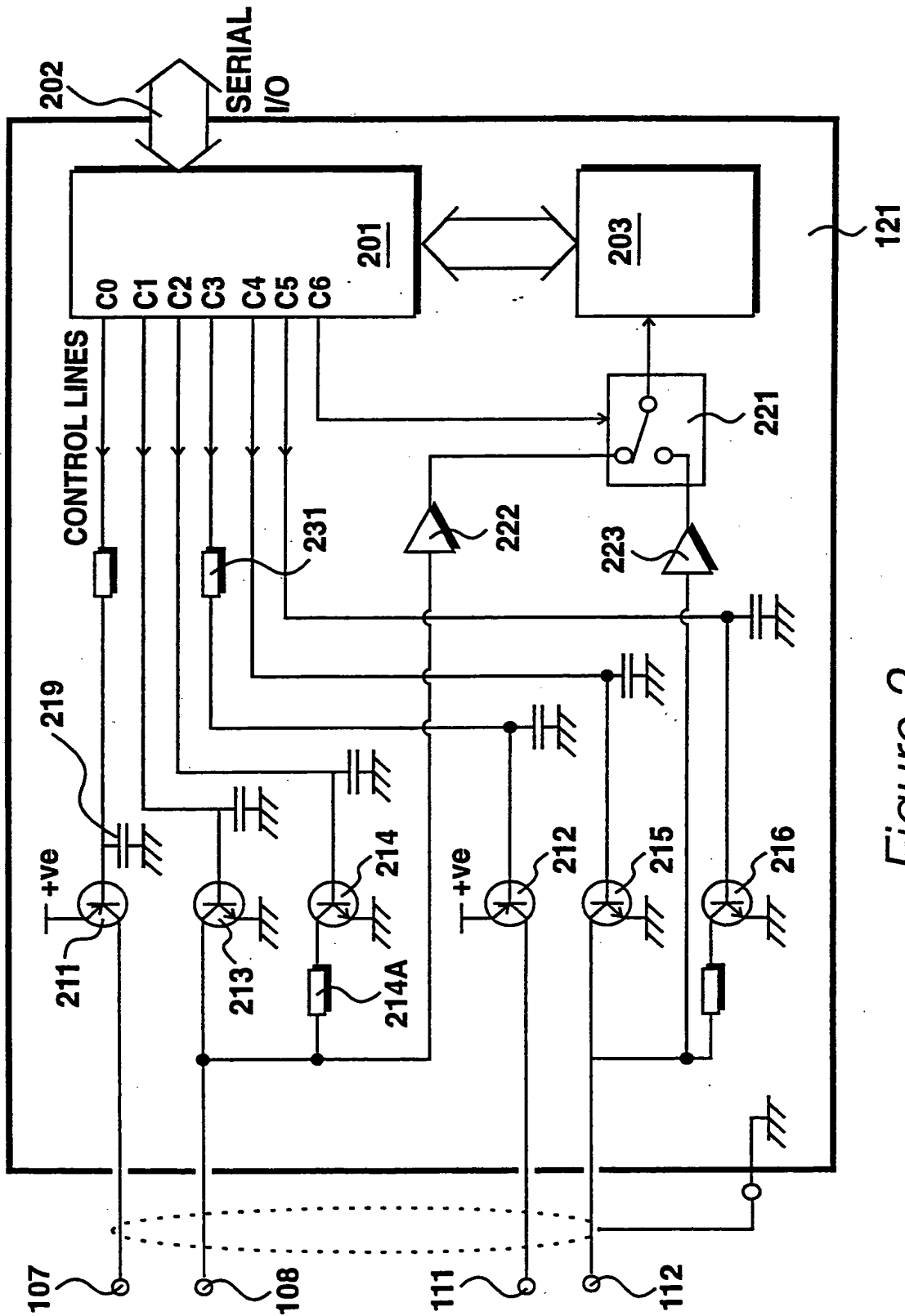
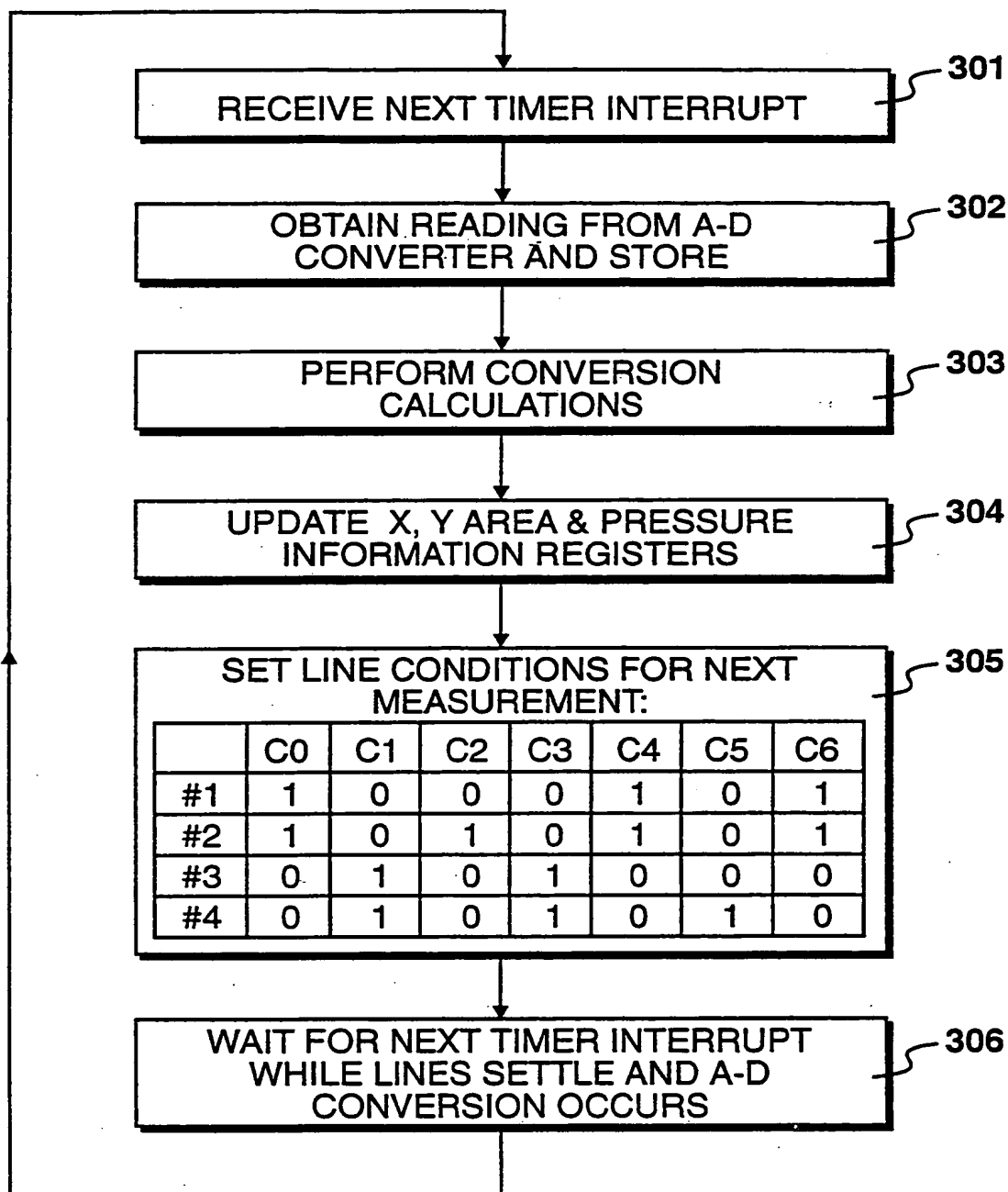


Figure 2

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*Figure 3*

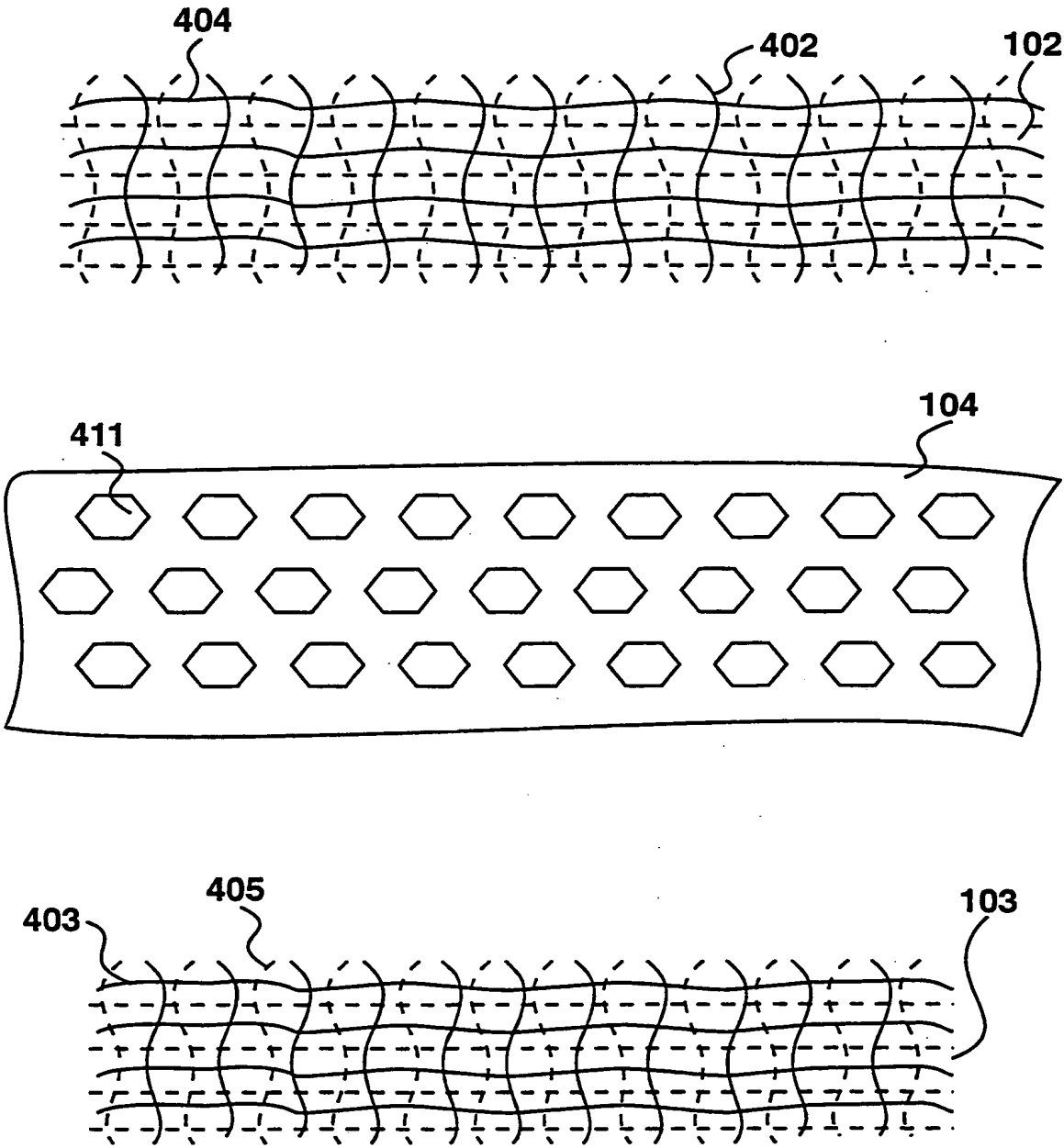


Figure 4

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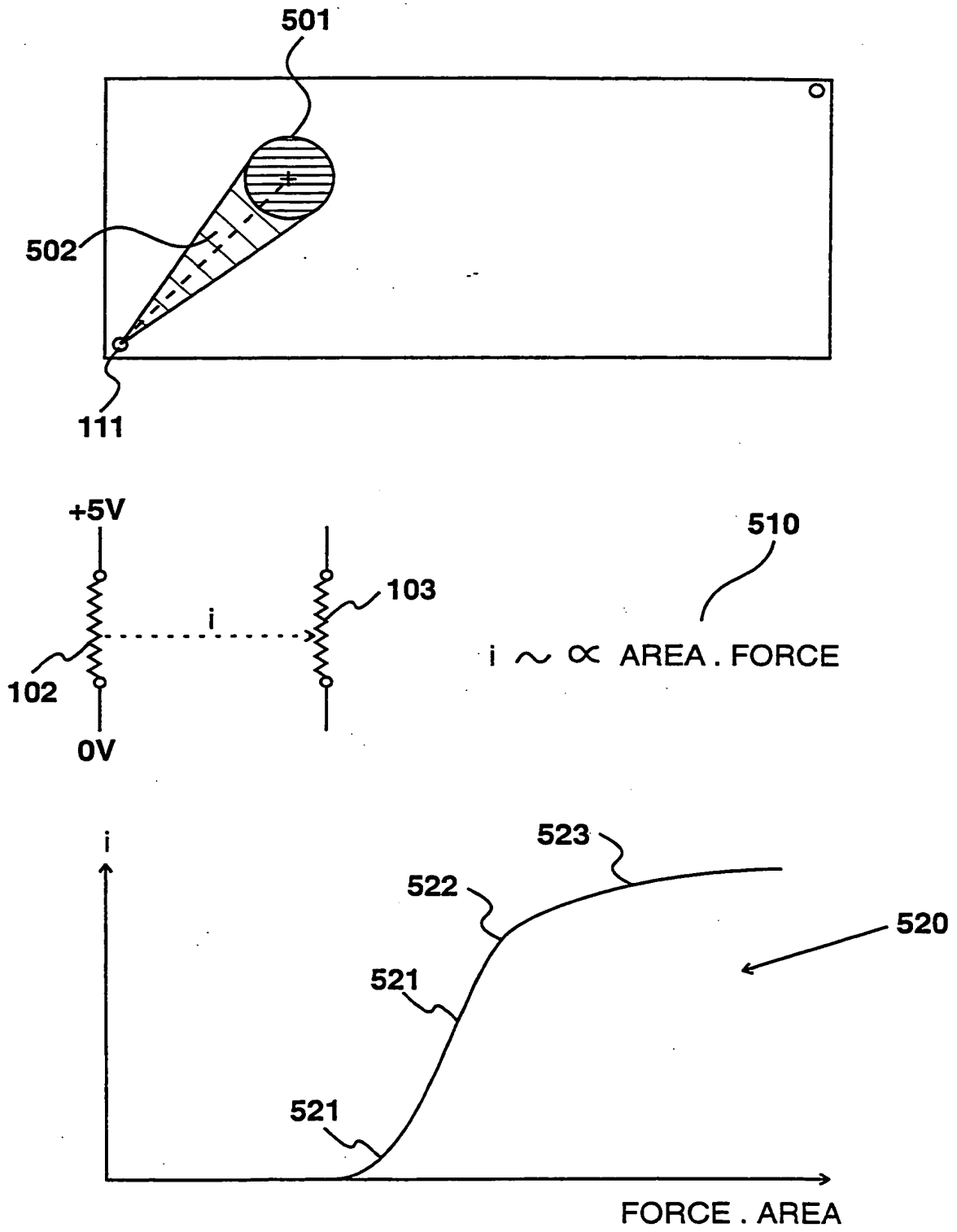


Figure 5

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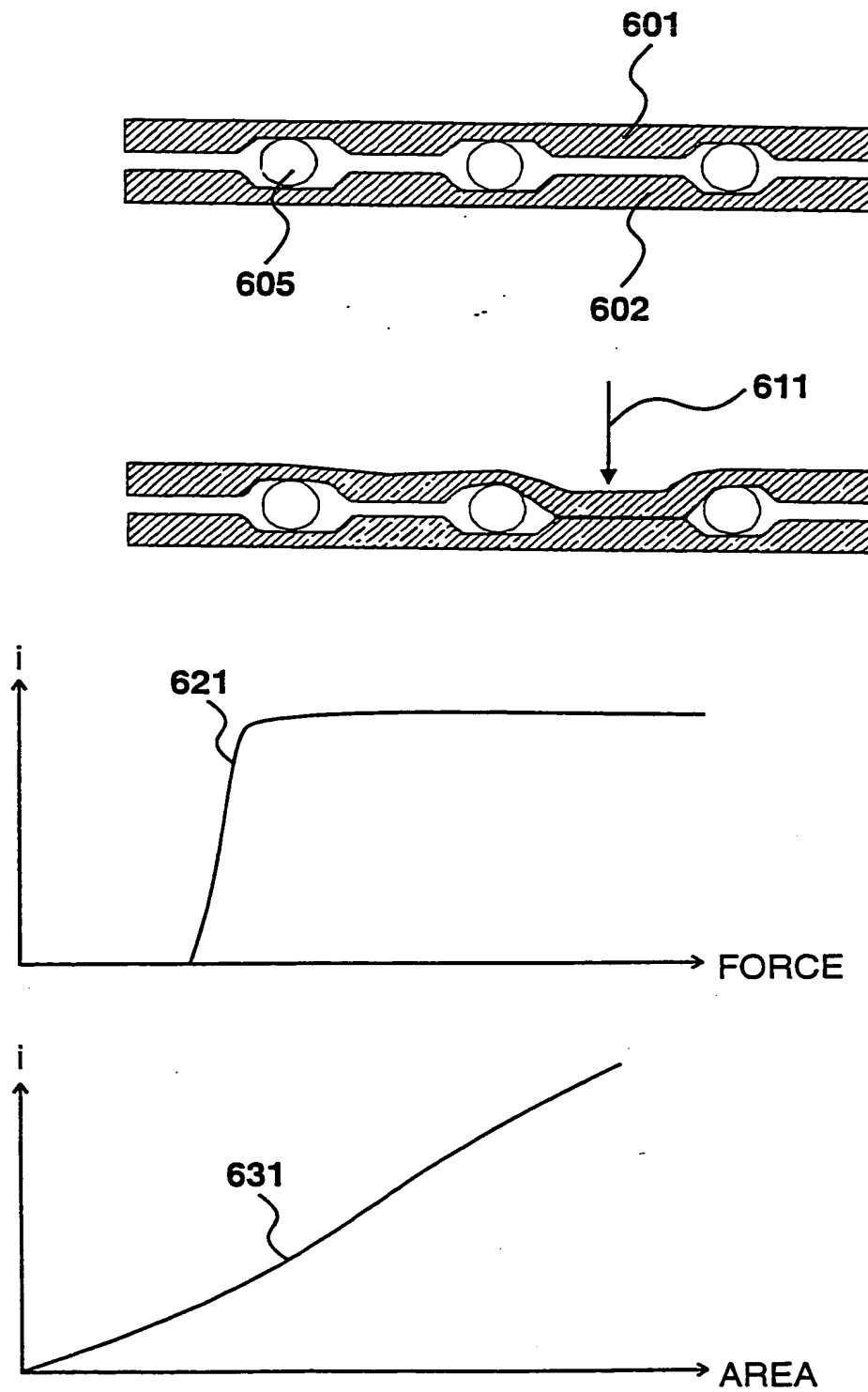


Figure 6

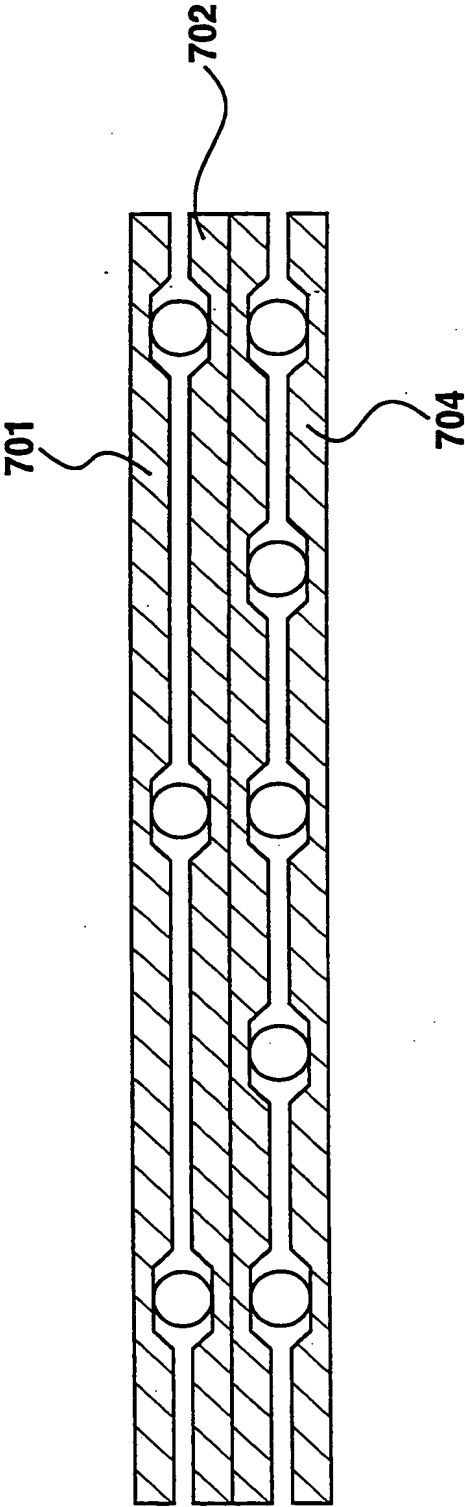


Figure 7



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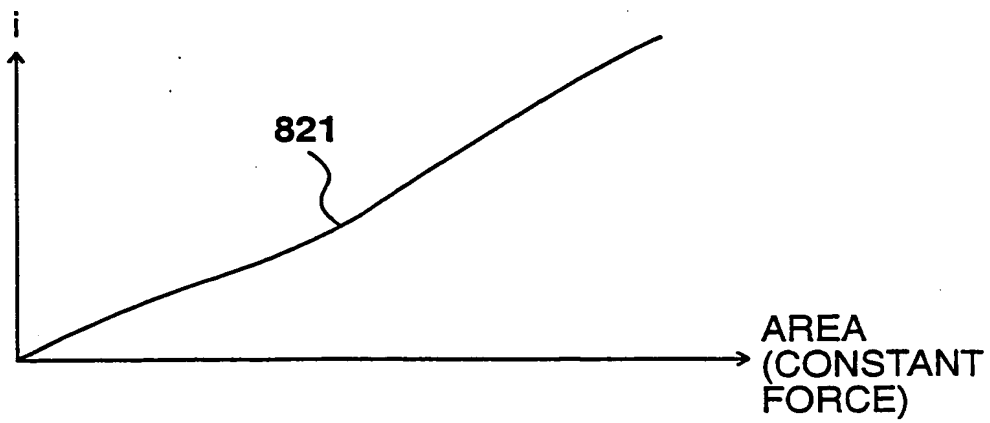
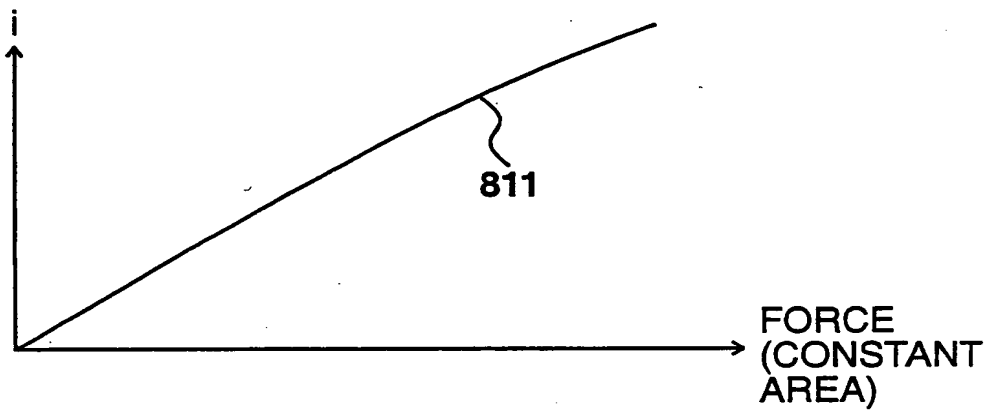
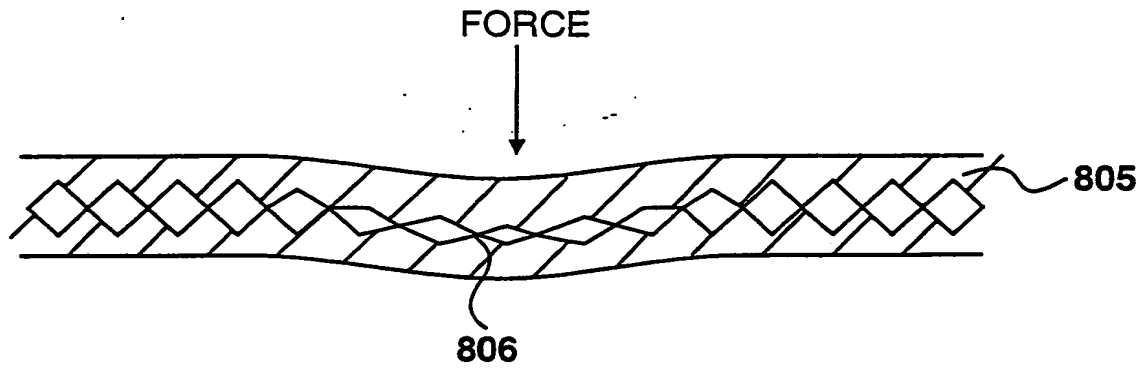
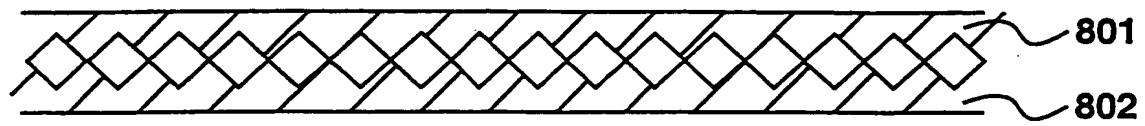
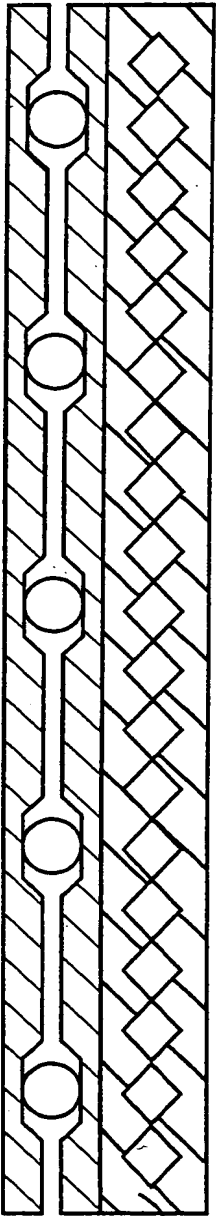


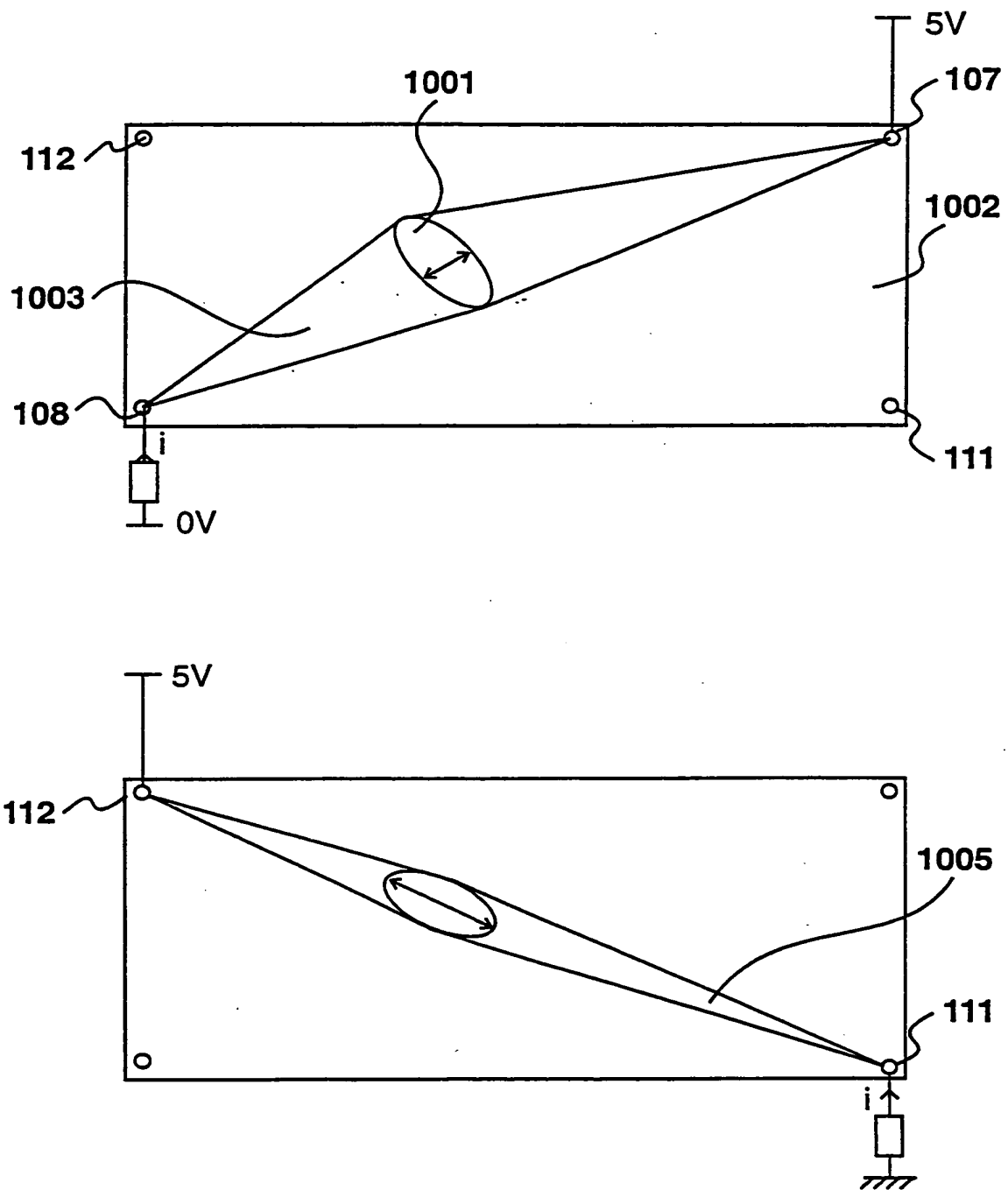
Figure 8



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Figure 9

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*Figure 10*

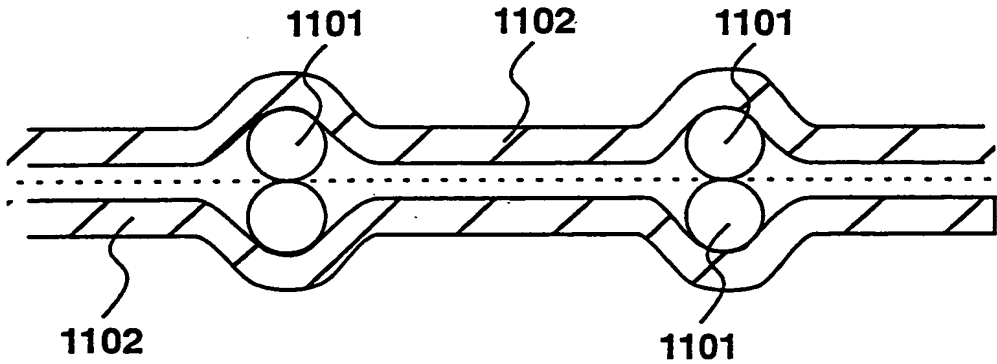


Figure 11A

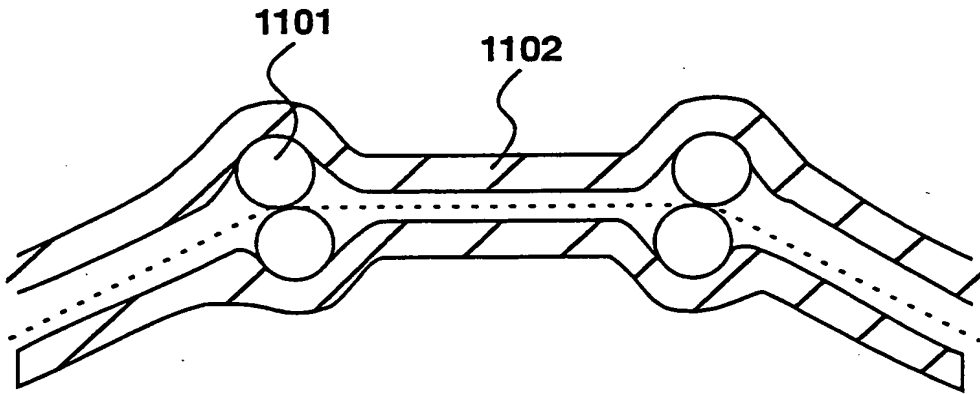
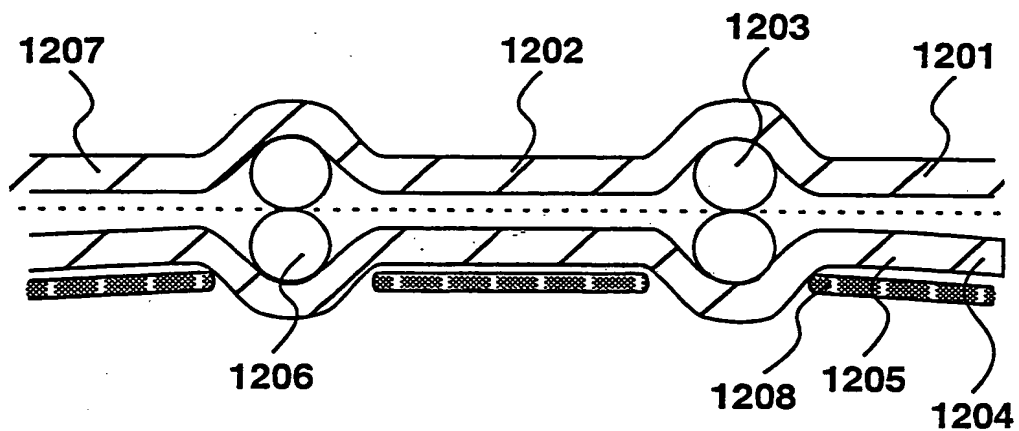
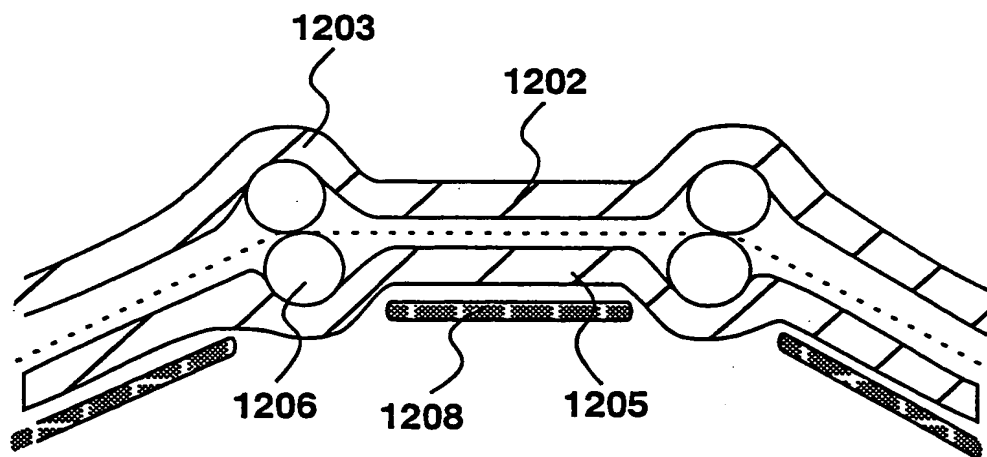


Figure 11B

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*Figure 12A*



*Figure 12B*

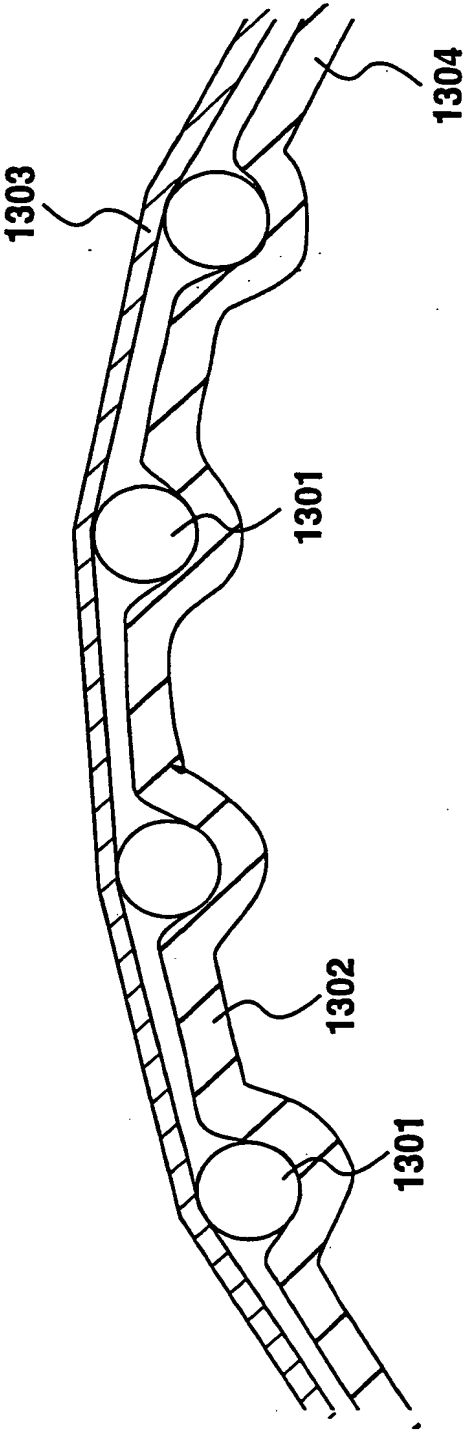


Figure 13

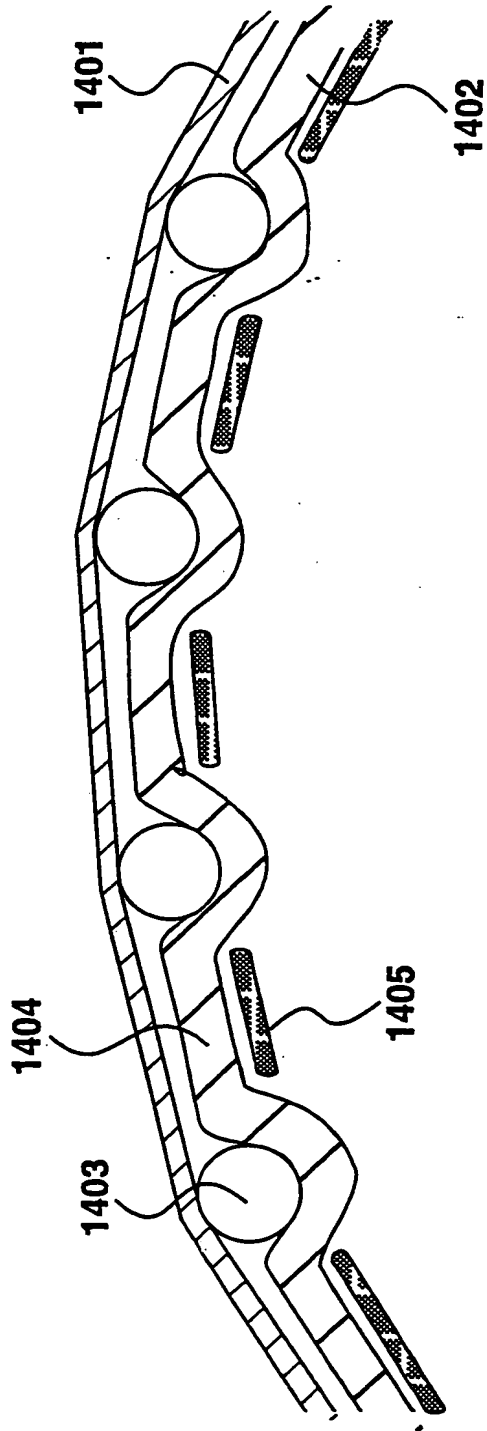


Figure 14

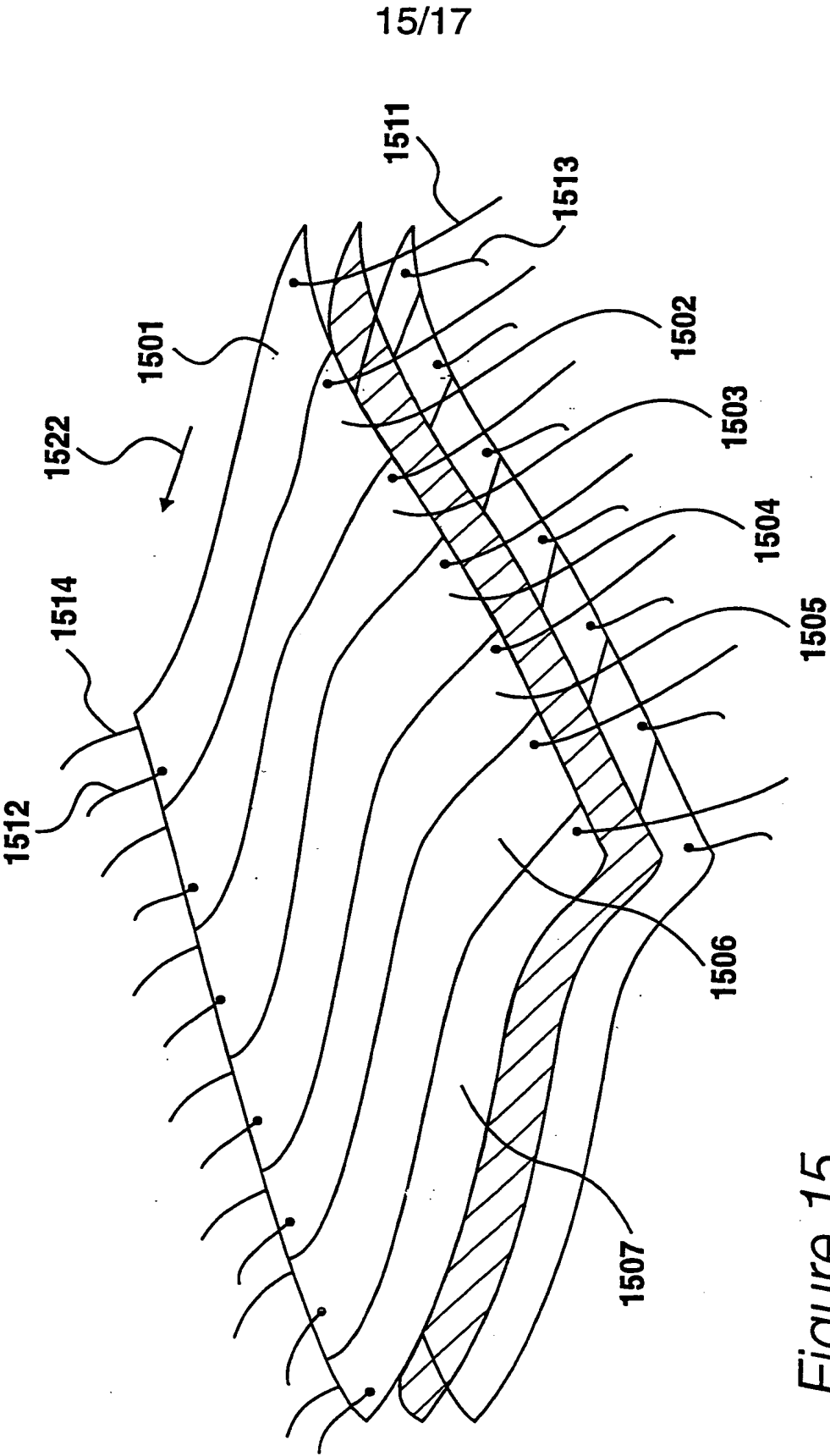


Figure 15



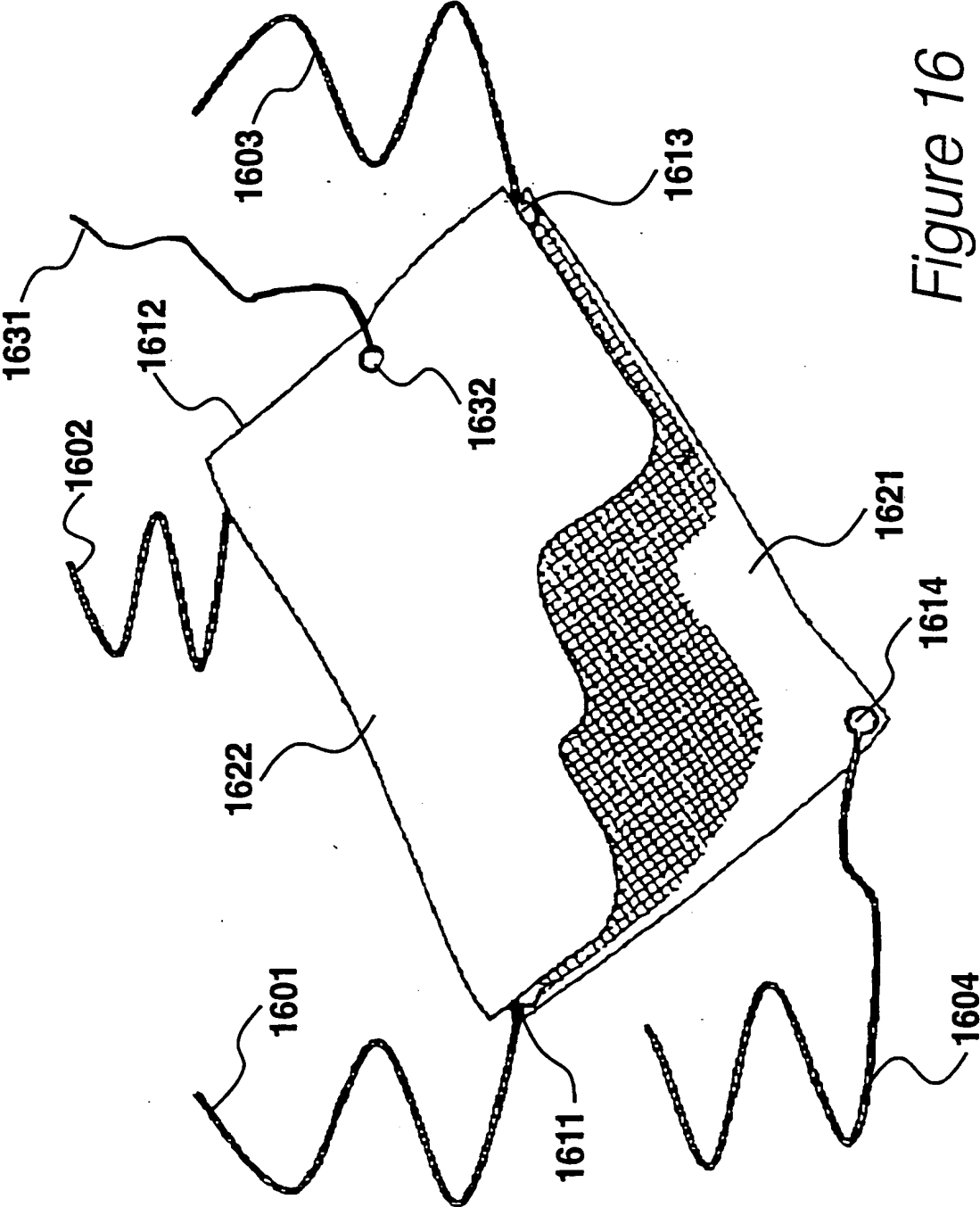


Figure 16

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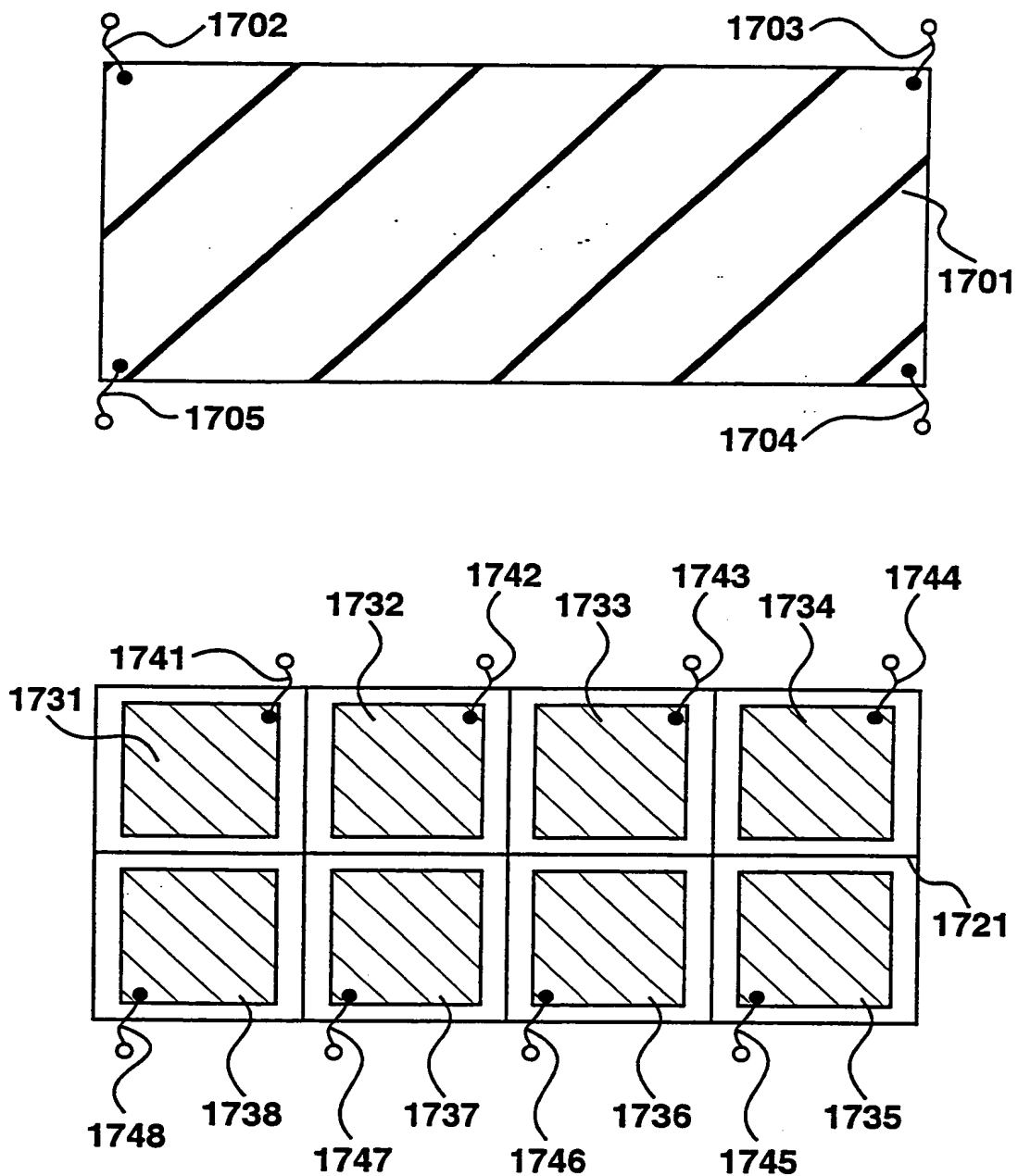


Figure 17

## Detector Constructed From Fabric

The present invention relates to a detector constructed from fabric having electrically conductive elements and configured to produce electrical outputs in response to mechanical interactions.

A fabric touch sensor for providing positional information is described in United States Patent 4,659,873 of Gibson. The sensor is fabricated using two layers of fabric having conducting threads, separated by a resistive layer to prevent unintentional contact.

An improvement to this proposal is disclosed in the applicant's co-pending British patent application number 98 20 902 in which there is provided a position detector constructed from fabric having electrically conductive elements, comprising at least two electrically conductive planes. A potential is applied across at least one of the planes to determine the position of a mechanical interaction. In addition, a second electrical property is determined, such as current, to identify additional properties to the mechanical interaction, such as an applied force, an applied pressure or an area of contact.

A further improvement is disclosed in the applicant's co-pending British patent application number 98 20 905, in which there is provided a detector constructed from fabric having electrically conductive elements to define at least two electrically conductive planes and configured to produce an electrical output in response to a mechanical interaction. At least one of the planes includes first portions and second portions, wherein the said first portions have a higher resistance than the second portions and the first higher resistance portions are more flexible than the second portions.

The second improvement provides the advantage of facilitating a folding or distortion of the detector whilst still maintaining full functionality.

According to a first aspect of the present invention, there is provided a detector constructed from fabric having electrically conductive elements and configured to produce electrical outputs in response to mechanical interactions, wherein a detector is divided into a plurality of regions; each of  
5 said regions includes a first conducting plane and a second conducting plane; and a mechanical interaction results in conducting planes of at least one of said regions being brought closer together.

In a preferred embodiment, one of said conducting planes is unique to a region and the co-operating conducting plane is shared with a plurality of  
10 regions. A single co-operating conducting plane may be shared with all of the regions.

Preferably, signals are derived independently from a plurality of regions by a time division multiplexing operation.

According to a second aspect of the present invention, there is  
15 provided a method of constructing a detector from fabric having electrically conductive elements and configured to produce electrical outputs in response to mechanical interactions, comprising the steps of dividing the detector into a plurality of regions; providing a first conductive plane and a second conductive plane for each of said regions; and bringing together conductive  
20 planes of at least one of said regions in response to a mechanical interaction.

The invention will be described by way of example only, with reference to the accompanying drawings of which:

*Figure 1* shows a position detector constructed from fabric;

*Figure 2* shows a control circuit identified in *Figure 1*;

25 *Figure 3* details operations performed by the micro-controller identified in *Figure 2*;

*Figure 4* details planes identified in *Figure 1*;

*Figure 5* details current flow due to mechanical interaction;

30 *Figure 6* details an alternative construction for conducting fabric planes;

*Figure 7* shows an alternative configuration of conducting planes;  
*Figure 8* shows an alternative configuration of conducting planes;  
*Figure 9* details a composite configuration of conducting planes; and  
*Figure 10* shows an asymmetric object interacting with conducting  
5 planes.

*Figure 11A* and *Figure 11B* show an alternative construction for a  
detector;

*Figure 12A* and *Figure 12B* show a further alternative construction;

*Figure 13* shows a further alternative construction;

*Figure 14* shows a further alternative construction.

*Figure 15* shows an alternative embodiment having a plurality of  
detectors;

*Figure 16* shows an alternative detector configuration; and

*Figure 17* shows multiple detectors of the type shown in *Figure 16*.

15 A position detector **101** constructed from fabric is shown in *Figure 1*.  
The detector has two electrically conducting fabric planes, in the form of a  
first plane **102** and a second plane **103**. The planes are separated from each  
other and thereby electrically insulated from each other, by means of an  
insulating mesh **104**. When force is applied to one of the planes, the two  
conducting planes are brought together, through the mesh **104**, thereby  
20 creating a position at which electrical current may conduct between planes  
**102** and **103**. In this way, it is possible to identify the occurrence and/or  
position of a mechanical interaction.

25 The fabric planes are defined by fabric structures, which may be  
considered as a woven, non-woven (felted) or knitted etc. The fabric layers  
may be manufactured separately and then combined to form the detector or  
the composite may be created as part of the mechanical construction  
process.

30 When a voltage is applied across terminals **107** and **108**, a voltage  
gradient appears over plane **102**. When a mechanical interaction takes place,

plane 103 is brought into electrical contact with plane 102 and the actual voltage applied to plane 103 will depend upon the position of the interaction. Similarly when a voltage is applied between connectors 111 and 112, a voltage gradient will appear across plane 103 and mechanical interaction will result in a voltage being applied to plane 102. Similarly, the actual voltage applied to plane 102 will depend upon the actual position of the interaction. In this way, for a particular mechanical interaction, it is possible to identify locations within the plane with reference to the two aforesaid measurements. Thus, connectors 107, 108, 111 and 112 are received by a control circuit 121, configured to apply voltage potentials to the detector 101 and to make measurements of electrical properties in response to mechanical interactions.

Control circuit 121 identifies electrical characteristics of the sensor 101 and in response to these calculations, data relating to the characteristics of the environment are supplied to a data processing system, such as a portable computer 131, via a conventional serial interface 131.

Control circuit 121 is detailed in *Figure 2*. The control circuit includes a micro-controller 201 such as a Philips 80C51 running at a clock frequency of twenty megahertz. Operations performed by micro-controller 201 are effected in response to internally stored commands held by an internal two kilobyte read-only memory. The micro-controller also includes one hundred and twenty-eight bytes of randomly accessible memory to facilitate intermediate storage while performing calculations. Micro-controller 201 includes a serial interface 202 in addition to assignable pins and an interface for communicating with an analogue to digital converter 203, arranged to convert input voltages into digital signals processable by the micro-controller 201.

The control circuit 121 includes two PNP transistors 211 and 212, in addition to four NPN transistors 213, 214, 215 and 216. All of the transistors are of relatively general purpose construction and control switching operations within the control circuit so as to control the application of voltages to the position detector 101.

In operation, measurements are made while a voltage is applied across first plane 102 and then additional measurements are made while a voltage is applied across the second plane 103; and output voltage only being applied to one of the planes at any particular time. When an output voltage is applied to one of the planes, plane 102 or plane 103, input signals are received from the co-operating plane 103 or 102 respectively. Input signals are received by the analogue to digital converter 203 via a selection switch 221, implemented as a CMOS switch, in response to a control signal received from pin C6 of the micro-controller 201. Thus, in its orientation shown in *Figure 2*, switch 221 has been placed in a condition to receive an output from a first high impedance buffer 222, buffering an input signal received from plane 102. Similarly, when switch 221 is placed in its alternative condition, an input is received from a second high impedance buffer 223, configured to receive an input signal from plane 103. By placing buffers 222 and 223 on the input side of CMOS switch 221, the switch is isolated from high voltage electrostatic discharges which may be generated in many conditions where the detector undergoes mechanical interactions.

In the condition shown in *Figure 2*, switch 221 is placed in its upper condition, receiving input signals from buffer 222, with output signals being supplied to the second plane 103. Further operation will be described with respect to this mode of operation and it should be appreciated that the roles of the transistor circuitry is reversed when switch 221 is placed in its alternative condition. As previously stated, condition selection is determined by an output signal from pin C6 of micro-controller 201. In its present condition the output from pin C6 is low and switch 221 is placed in its alternative configuration when the output from pin 6 is high.

Output pin C0 controls the conductivity of transistor 211 with pins C1 to C5 having similar conductivity control upon transistors 212, 213, 214, 215 and 216 respectively.

Transistors **211** and **213** are switched on when a voltage is being applied to the first plane **102** and are switched off when a voltage is being applied to the second plane **103**. Similarly, when a voltage is being applied to the second plane **103**, transistors **212** and **215** are switched on with transistors **211** and **213** being switched off. In the configuration shown in *Figure 2*, with switch **221** receiving an input from buffer **222**, output transistors **211** and **213** are switched off with output transistors **212** and **215** being switched on. This is achieved by output pin C0 being placed in a high condition and pin C1 being placed in a low condition. Similarly, pin C3 is placed in a low condition and pin C4 is placed in a high condition.

In the configuration shown, C3 is placed in a low condition, as previously described. The micro-controller **201** includes a pull-down transistor arranged to sink current from the base of transistor **212**, resulting in transistor **212** being switched on to saturation. Consequently, transistor **212** appears as having a very low resistance, thereby placing terminal **111** at the supply voltage of five volts. Resistor **231** (4K7) limits the flow of current out of the micro-controller **201**, thereby preventing burn-out of the micro-controller's output transistor.

Pin C4 is placed in a high state, resulting in transistor **215** being placed in a conducting condition. A serial resistor is not required given that the micro-controller **201** includes internal pull-up resistors, as distinct from a pull-up transistor, such that current flow is restricted. Thus, transistors **212** and **215** are both rendered conductive, resulting in terminal **111** being placed at the positive supply rail voltage and terminal **112** being placed at ground voltage. The capacitors shown in the circuit, such as capacitor **219**, limit the rate of transistor transitions thereby reducing rf transmissions from the sensor **101**.

With transistors **212** and **215** placed in their conductive condition, input signals are received from the first plane **102** in the form of a voltage applied to terminal **108**. For position detection, this voltage is measured



directly and transistor **214** is placed in a non-conductive condition by output pin C2 being placed in a low condition. Under these conditions, the voltage from input terminal **108** is applied to analogue to digital converter **203** via buffer **222** and switch **221**.

5 In accordance with the present invention, a second electrical property is determined which, in this embodiment, represents the current flowing through the sensor in response to a mechanical interaction. The current measurement is made by placing transistor **215** in a conductive condition, by placing output pin C4 in a high condition. In this condition, current received at  
10 terminal **108** is supplied to transistor **214** via resistor **214A**, having a resistance of typically 5k selectable so as to correspond to the characteristics of the sensor. A voltage is supplied to A to D converter **203** via buffer **222** and switch **221** but on this occasion the voltage represents a voltage drop, and hence a current, across resistor **214A**.

15 Thus, transistors **212** and **215** are placed in a conducting condition, transistor **214** is placed in a non-conducting condition, so as to measure voltage, and is then placed in a conducting condition so as to measure current. The roles of the transistors are then reversed, such that output transistors **211** and **213** are placed in a conducting condition, with transistors  
20 **212** and **215** being placed in a non-conducting condition (and switch **221** reversed) allowing a voltage to be measured by placing transistor **216** in a non-conducting condition, and then allowing a current to be measured by placing transistor **216** in a conducting condition.

The cycling of line conditions, in order to make the measurements  
25 identified previously, is controlled by a clock resident within micro-controller **201**. After each condition has been set up, a twelve bit number is received from the digital to analogue converter **203** and this number is retained within a respective register within micro-controller **201**. Thus, after completing a cycle of four measurements, four twelve bit values are stored within the  
30 micro-controller **201** for interrogation by the processing device **131**.

Furthermore, the rate of cycling may be controlled in response to instructions received from the processing device 131.

Operations performed by micro-controller 201 are detailed in *Figure 3*. The micro-controller continually cycles between its four configuration states and each time a new input is produced, representing a current or a voltage in one of the two configurations, new output data is calculated on an on-going basis. Thus, output registers are updated such that the best data is made available if the micro-controller is interrupted by the external processor 131.

The micro-controller 201 is fully interrupt driven in terms of receiving external interrupts for data interrogation along with internal interrupts in order to initiate a configuration cycle. The external interrupt has a higher priority such that external processor 131 is provided with information as soon as possible in response to making an interrupt request.

Internally interrupts for the micro-controller 201 are generated by its own internal timer and the procedure shown in *Figure 3* is effectively held in a wait state until a next timer interrupt is received at step 301. The wait state allows voltage levels on connections 107, 108, 111 and 112 to become stable and provides sufficient time for valid data to be received from the analogue to digital converter 203.

At step 302, an output is received from analogue to digital converter 203 and at step 303 calculations are performed with respect to the most current data received from the analogue to digital converter, so as to convert numerical values relating to voltages and currents into numerical values representing properties of the mechanical interaction. Thus, after performing calculations at step 303, appropriate registers are updated at step 304 and it is these registers that are interrogated in response to an interrupt received from processing system 131.

At step 305 next conditions for the output lines are set by appropriate logic levels being established for output pins C0 to C6. After the next output condition has been selected, the processor enters a wait state at step 306,

allowing the electrical characteristics to settle, whereafter processing continues in response to the next timer interrupt.

Thus, it should be appreciated that on each iteration of the procedure shown in *Figure 3*, one of the output conditions is selected at step 305. Thus, it should be appreciated that the input data is effectively delayed and does not represent a condition of the electrical characteristics at an instant. If in practice, the delay between measurements becomes too large, it becomes necessary to enhance the frequency of operation of circuits within the control system shown in *Figure 2*. Thus, the rate of conversion for converter 203 would need to be increased and the circuitry would need to be redesigned for high frequency operation. This in turn could create problems in terms of high frequency interference resulting in enhanced shielding being required for the facility as a whole.

When output condition number one is selected, an output voltage at 108 is determined. On the next cycle, identified as output condition number two, the current flowing through connector 108 is determined. On the next iteration, under output configuration number three, the voltage appearing at connector 112 is determined and on the next cycle, identified as condition number four, the current flowing through connector 112 is determined. After each of these individual measurements, new data is generated in response to steps 303 and 304 such that resulting output registers are being regularly updated on a continual basis, such that the processing system 131 may effectively perform a continual monitoring operation in terms of changes made to the mechanical interactions with the detector 101.

In a typical implementation, the four characteristic measurements, making up a complete cycle, will be repeated at a frequency of between twenty-five to fifty times per second. In situations where such a repetition rate is not required, it may be preferable to increase the duration of the wait states and thereby significantly reduce overall power consumption.

Planes 102, 103 and 104 of the detector 101 are detailed in *Figure 4*. Planes 101 and 103 are of substantially similar construction and are constructed from fabric having electrically conductive elements 402 in plane 102 along with similar electrical conductive elements 403 in plane 103. Thus, it is possible for a voltage indicative of position to be determined when conductive elements 402 are placed in physical contact with conductive elements 403.

The overall resistivity of planes 402 and 403 are controlled by the inclusion of non-conducting elements 404 and 405. Thus, resistivity is controlled by controlling the relative quantities and/or densities of conductive elements 402 with non-conductive elements 404. Resistivity may also be controlled by selecting an appropriate fibre type, adjusting the thickness of the fibre or adjusting the number of strands present in a yarn.

Plane 404 represents a non-conducting insulating spacer positioned between the two conducting planes 102 and 103. Plane 104 is constructed as a moulded or woven nylon sheet having an array of substantially hexagonal holes 411, the size of holes 411 is chosen so as to control the ease with which it is possible to bring conductive elements 402 into physical contact with conductive elements 403. Thus, if relatively small holes 411 are chosen, a greater force is required in order to bring the conductive elements together. Similarly, if the size of the hole is increased, less force is required in order to achieve the conductive effect. Thus, the size of holes 411 would be chosen so as to provide optimal operating conditions for a particular application. Operating conditions may also be adjusted by controlling the thickness of layer 104, its surface flexibility and the contour of co-operating planes 102 and 103.

When a potential is applied across one of the conducting planes, the actual potential detected at a point on that plane will be related to the position at which the measurement is made. Thus, a direct voltage measurement from the co-operating plane gives a value from which a positional co-ordinate

may be determined. By reversing the plurality of the planes and taking a measurement from the opposing plane, two co-ordinates are obtained from which it is then possible to identify a precise location over the planar surface.

In addition to measuring position on the planar surface, the present invention is directed at identifying additional electrical properties in order to determine properties of the mechanical interaction. As previously described, the system is configured to measure currents in addition to measuring voltages.

When the two conducting planes are brought into mechanical contact, due to a mechanical interaction, the amount of current flowing as a result of this contact will vary in dependence upon the actual position of the plane where the mechanical interaction takes place. The position of the mechanical interaction has also been determined with reference to voltages and it could be expected that these two quantities will vary in a substantially similar way, each representing the same physical situation. Experience has shown that variations in measured current do not follow exactly the same characteristic as variations in measured voltage. As illustrated in *Figure 5*, the amount of current flowing due to a mechanical interaction will depend upon the position of a mechanical interaction 501. However, in addition to this, the amount of current flow will also depend upon the size of the mechanical interaction. As the size of the mechanical interaction increases, there is a greater area of contact and as such the overall resistance of the mechanical interaction is reduced. However, it should be appreciated that variations in terms of current with respect to interaction size is a sophisticated relationship, given that, in addition to the resistivity of the contact area 501, the resistivity of the actual electrical connections within the sheet must also be taken into account.

Thus, current is transmitted through a region 502 in order to provide a current to the contact region 501. Some aspects of this effect will be compensated with reference to position calculations and other variations due to this effect may be compensated by a non-linear analysis of the input data.

Contact area resistivity is illustrated generally at 510 and shows that the amount of current flowing between plane 102 and plane 103 is considered as being related to the area of mechanical interaction, which is related to the area of contact externally and to the level of externally applied mechanical force.

The resulting non-linear relationship between the force area product and the resulting current flow is illustrated generally at 520. At 521 there is an initial threshold point, identifying the point at which the gap starts to be closed, followed by an operational part of the curve which may give useful indications of pressure up to point 522, whereafter the relationship becomes very non-linear until position 523 where the relationship effectively saturates.

Using a detector of the type illustrated in *Figure 1*, it is possible to measure current flow, which could also be considered as contact resistance, in order to identify an additional mechanical property of the interaction. As illustrated in *Figure 5*, this other mechanical property is related to the area of contact between the sheets, determined by the amount of force applied to the sheets, and to the total area over which the force is applied; or a combination of these two properties. Thus, data relating to force and area may give useful information relating to the interaction, separate from the position at which the interaction takes place.

In some situations, such as when using a stylus or similar implement, the area of applied force remains substantially constant therefore a measurement of current will enable calculations to be made in terms of stylus pressure. Pressure sensitive styli are known but in known configurations the pressure detection is determined within the stylus itself, leading to the stylus being mechanically connected to operational equipment or requiring sophisticated wireless transmission within the stylus itself. The present embodiment allows stylus pressure to be determined using any non-sophisticated stylus, given that the pressure detection is made by the co-operating fabric detector, arranged to detect stylus position (with reference to

voltage) in combination with stylus pressure, with reference to current.

An alternative construction for the conducting fabric planes is illustrated in *Figure 6*. The detector includes a first conducting plane **601** and a second conducting plane **602**. In addition, woven into each of the conducting planes **601** and **602**, there are a plurality of non-conducting nodes **605** arranged to mutually interfere and thereby separate the two conducting planes. Between the nodes, the fabrics of the first and second planes may be brought into contact relatively easily such that the application of force, illustrated by arrow **611** would tend to cause a finite number of regions interspersed between nodes **605** to be brought into contact. Thus, for a particular region, contact either is taking place or is not taking place as illustrated by curve **621**.

With a number of such regions brought into contact, the overall level of current flow will tend to vary with the area of contact as illustrated by curve **631**. Thus, using a construction of the type shown in *Figure 6*, it is possible to obtain a more linear relationship, compared to that shown in *Figure 5*, in which the level of current flow gives a very good indication of the area of coverage as distinct from the level of force applied to the mechanical interaction.

Given a construction of the type shown in *Figure 6*, an indication of applied force or pressure may be obtained, in addition to an accurate determination of area, by providing an incremental switching operation. In the configuration shown in *Figure 7*, there is provided a first conducting plane **701** which interacts with a second conducting plane **702**. Furthermore, conducting plane **702** interacts with a third conducting plane **704**. Conducting plane **701** is separated from conducting plane **702** by non-conducting portions **705**. Similarly, plane **702** is separated from plane **704** by non-conducting portions **706**. More non-conducting portions **705** are provided than similar non-conducting portions **706**. Consequently, less force is required to produce electrical contact between planes **701** and **702** than is

required to produce an electrical contact between planes 702 and 704. In this way, it is possible to provide an incremental measurement of force, given that a low force will only cause contact between plane 701 and plane 702 whereas a larger force will also provide electrical contact between plane 702 and 704.

An alternative configuration is shown in *Figure 8* in which it is possible to obtain enhanced substantially continuous variations in current flow with respect to applied force. A first conducting plane 801 interacts with a second conducting plane 802. The planes are woven in such a way as to produce very uneven surfaces such that, under light load, the level of interaction is relatively low. As load increases, as illustrated generally at 805, a greater level of surface contact shown at 806 is created thereby increasing the level of current flow in a substantially continuous way. It should also be noted that this configuration does not include an insulating layer as such and that a level of current flow will always take place even under conditions of zero load. Alternatively, a very thin insulating layer could be provided, having a relatively low threshold, thereby resulting in a zero current flow when no load is applied.

As shown by curve 811, the output current varies with respect to variations in applied force for a constant load area. Similarly, as shown by curve 821, output current varies with respect to load area for a substantially constant applied force.

A composite configuration is shown in *Figure 9*, in which a detector 901, substantially similar to that shown in *Figure 6*, is combined with a detector 902, substantially similar to that shown in *Figure 9*. Detector 901 provides an accurate measurement of applied area and it is relatively unaffected by applied force. Detector 902, as shown in *Figure 8*, provides an output which varies with respect to area and force. Thus, by processing the output of these two detectors in combination, it is possible to compensate the output from detector 902 in order to produce values representing force, such



that the two currents provide indications of both force and area.

The operation of the control circuit 121 is such as to apply a first voltage across diagonals 107 and 108 with a similar voltage being applied across diagonals 111 and 112. The nature of the voltage distribution is therefore asymmetric, but this does not result in difficulties provided that the area of contact between the two planes is relatively symmetric. However, should an asymmetric area of contact be made, as illustrated in *Figure 10*, differences will occur in terms of current measurements when considering calculations made in the two directions.

An asymmetric object 1001 is shown applied to the surface of a detector 1002. When a voltage is applied between contact 107 and 108, paths over which current may flow, illustrated generally at 1003 are relatively large and the object is perceived as having a large area or is perceived as applying a large force. In the opposite dimension, when a voltage is applied between 111 and 112, the regions over which current flow takes place illustrated generally at 1105, become relatively smaller therefore the object would be perceived as having a relatively smaller area or would be perceived as providing a relatively smaller force.

If the system is programmed to the effect that the object has a constant area and applies a constant force, these differences in terms of current flow may be processed in order to give an indication as to the orientation of the object. Thus, the system of the type illustrated in *Figure 10*, is used in combination with the detector of the type illustrated in *Figure 9* it is possible to make reference to the parameters of location in two-dimensions, force or pressure, the area of application and orientation.

In the preferred embodiment, electrical characteristics of voltage and current are measured. Alternatively, it would be possible to determine the resistance or the resistivity of the conducting sheets. Problems may be encountered when using alternating currents due to energy being radiated from the conducting sheets. However, in some situations it may be preferable

to use alternating currents, in which further electrical characteristics of the detector may be considered, such as capacitance, inductance and reactance etc.

5 The detector shown in *Figure 1*, constructed from conducting planes **102** and **103**, operates satisfactorily if the plane of the detector is maintained substantially flat. This does not create a problem in many applications where relatively flat operation is considered desirable. However, although constructed from fabric, thereby facilitating bending and folding operations, the reliability of the detector in terms of its electrical characteristics cannot be  
10 guaranteed if the detector planes are folded or distorted beyond modest operational conditions.

A detector is shown in *Figure 11*, constructed from fabric having electrically conductive elements to define at least two electrically conductive planes. The detector is configured to produce an electrical output in response  
15 to a mechanical interaction, as illustrated in *Figure 1*. At least one of the planes includes first portions and second portions in which the first portions have a higher resistance than said second portions and the first higher resistance portions are more flexible than the second portions. In this way, flexing occurs at the portions of high resistance, where contact between the  
20 planes has little effect, while the lower resistance portions, where contact does have a strong electrical effect, remain substantially rigid such that the flexing of the material does not occur over these portions of the detector.

Portions **1101** have a relatively high resistance compared to portions **1102**. Portions **1101** are not involved in terms of creating an electrical  
25 reaction in response to a mechanical interaction. The electrical responses are provided by the more rigid weave of portions **1102**. The purpose of portions **1101** is detailed in *Figure 11B*. A curvature has been applied to the detector but the configuration is such that normal operation is still possible. The flexing has occurred predominantly at portions **1101**. However, portions **1102** have  
30 remained straight thereby ensuring that they remain displaced from each

other, even when a curvature is present, such that the detector is still available for detecting the presence of a mechanical interaction.

The rigidity of portions 1102 may be enhanced as shown in *Figure 12A*. A first plane 1201 has rigid portions 1202 and flexible portions 1203. A second plane 1204 has relatively rigid portions 1205 and relatively flexible portions 1206. The relatively flexible portions 1206 physically contact against similar portions 1203 in the first plane 1201. In order to ensure that there is no, or at least minimal electrical interaction at these points of contacts, the electrical resistance of the flexible portions 1203 and 1206 is relatively high. A partially insulating layer may be provided between the conducting layers, as shown in *Figure 1*. However, the flexible portions 1203 act as insulating separators therefore in this embodiment the provision of a separation layer is not essential. Furthermore, the rigidity of the interacting sections, in terms of the rigid portions 1202 and 1205, has its rigidity further enhanced by the presence of relatively solid intermediate plates 1208.

Flexing of the construction shown in *Figure 12A* is substantially similar to that provided by the embodiment shown in *Figure 11B*. The flexing of the embodiment shown in *Figure 12A* is detailed in *Figure 12B*. Flexing occurs at the position of the relatively flexible portions 1203 and 1206. The rigidity of portions 1202 and 1205 is enhanced by the provision of more solid plates 1208. Thus, the embodiment shown in *Figures 12A* and *12B* may have more strenuous flexing forces applied thereto such that mechanical interaction detection is maintained even under severe operating conditions.

The provision of the flexible portions effectively provide lines over the surface of the conducting planes where folding is permitted. Thus, complex curvatures may be obtained by a number of folds being effected at a plurality of these preferred foldable lines, thereby allowing complex shapes to be attained while maintaining the desired electrical characteristics.

An alternative embodiment is shown in *Figure 13* in which a first co-operating plane has flexible high resistive portions 1301 and rigid conducting

portions 1302. This plane co-operates with a second plane 1303 of substantially homogenous construction. Thus, sufficient flexing and insulation is provided by the non-conducting flexible portions 1301 of the lower co-operating plane 1304. The rigidity of conducting portions 1302 may be enhanced in a fashion substantially similar to that provided by *Figure 12A* as illustrated in *Figure 14*. The device includes an outer plane 1401 of substantially homogenous conducting construction. Below this, there is provided a second co-operating plane 1402 and the two planes may be separated by an insulating layer not shown in the example. The second plane or layer includes flexible non-conducting portions 1403 and more rigid conducting portions 1404, substantially similar to those shown in *Figure 13*. In addition, rigid plates 1405 are provided below each rigid portion 1404 thereby significantly enhancing the rigidity of these portions. Thus, the construction in *Figure 4* is capable of withstanding more aggressive working environments compared to the lighter construction shown in *Figure 13*.

In the construction shown in *Figures 13* and *14* the outer layers, 1303 and 1401 respectively, are fabricated in a substantially elastic fashion, thereby providing for a stretching or extension of this layer during flexing operations.

The detector shown in *Figure 1* is capable of accurately detecting the position of a mechanical interaction and as previously described, it is also possible to determine other characteristics of the mechanical interaction by modifying other electrical properties. A problem with the detector shown in *Figure 1* is that it experiences difficulties if more than one unconnected mechanical interaction takes place. If a first mechanical interaction were to take place and, simultaneously, a second mechanical interaction were to take place, displaced from the first, it would not be possible, using the configuration shown in *Figure 1*, to identify the presence of two mechanical interactions. A condition would be detected to the effect that a mechanical interaction is taking place but the system would tend to perceive this as a

single mechanical interaction having characteristics substantially similar to the average of the characteristics of the two independent interactions.

An alternative embodiment for overcoming problems of this type is shown in *Figure 15*. In *Figure 15*, a plurality of detectors **1501**, **1502**, **1503**, **1504**, **1505**, **1506** and **1507** have been connected together and each of these individual detectors has its own unique connectors **1511**, **1512**, **1513** and **1514**. In this way, each of the individual detectors may be connected to its own respective control circuit, such as circuit **121** shown in *Figure 1* or, in an alternative embodiment, a single control circuit of the type shown in *Figure 1* may be shared, using a switching arrangement, between all seven of the individual combined detectors. In this way, each individual detector, such as detector **1501**, provides the same level of accuracy as the detector shown in *Figure 1*. However, if two or more mechanical interactions take place on different detector sections, it is possible to detect this condition and provide appropriate output responses. However, it is only possible to detect a plurality of mechanical interactions if these interactions take place on different sections and it is not possible for the embodiment shown in *Figure 15* to detect a plurality of interactions if these interactions take place on the same section.

In the arrangement shown in *Figure 15*, the detectors have been arranged in strips such that there is enhanced definition in the direction of arrow **1521** but the definition in the direction of arrow **1522** has not changed.

In the detector shown in *Figure 1*, position detection is made possible using four electrical connection cables, a first two connected to opposing diagonal corners of the upper sheet and a further two connected to the alternative opposing diagonal corners of the lower sheet. An alternative configuration is shown in *Figure 16* in which electrical connectors **1601**, **1602**, **1603** and **1604** are connected to respective corners **1611**, **1612**, **1613** and **1614** of a lower plane conducting sheet

1621. An upper plane conducting sheet 1622 is connected to a single detecting cable 1631 connected at a position 1632 towards an edge of upper conducting sheet 1622. A disadvantage of the configuration shown in *Figure 16* is that five separate electrical connections are required whereas only four electrical connections are required in the configuration shown in *Figure 1*. However, in some circumstances, the configuration shown in *Figure 16* does have advantages over that shown in *Figure 1*.

The configuration shown in *Figure 16* may be used to effectively multiplex the operation of a detector so as to facilitate the detection of a plurality of mechanical interactions to a greater extent than the configuration shown in *Figure 15*. In particular, it facilitates detecting multiple mechanical interactions in both dimensions of the planar detector.

As shown in *Figure 17*, a lower planar sheet 1701 has connections 1702, 1703, 1704 and 1705 at each of its corners. Thus, sheet 1701 operates in a way which is substantially similar to the operation of sheet 1621 and all output voltages are generated within this sheet, either across diagonal 1702 to 1704 or across diagonal 1703 to 1705, thereby giving a two-dimensional co-ordinate within the area of the sheet.

An upper planar sheet 1721 is divided into a plurality of portions. In the example shown, eight portions 1731 to 1738 are provided. Thus, the mechanical action results in conducting planes of at least one of said regions being brought into electrical interaction with the lower plane 1701. Furthermore, if a mechanical interaction occurs at region 1731 and a second mechanical interaction occurs at region 1735 (for example) both of these mechanical interactions may be determined independently and an output to this effect may be generated by a processing system, such as system 131.

In order to achieve the space division multiplexing provided by regions 1731 to 1738, time division multiplexing of the electrical signals is performed in which, during each individual time slot, one individual region

1731 to 1738 is considered. This is achieved by each individual region 1731 to 1738 having its own respective electrical connector 1741 to 1748. These connectors are preferably incorporated in to the structure of the sheet.

5           Control circuitry for the configuration shown in *Figure 17* requires modification compared to that shown in *Figure 2*. In particular, each of the eight output control lines 1741 is supplied to its own respective buffering amplifier, similar to amplifiers 2223 and 2223 and the output from each of these eight amplifiers is applied to appropriate switching devices, allowing  
10           one of eight inputs to be selected using a plurality of switches substantially similar to switch 2221.

          A complete scanning cycle consists of applying a voltage between input terminals 1702 and 1704. An output is then considered from each individual output terminals 1741 to 1748. The voltages are then reversed  
15           such that a voltage is applied between output terminals 1705 and 1703. Each of the individual input terminals is then considered again so as to provide two-dimensional co-ordinates within each of the individual regions 1731 to 1748. As described with respect to *Figure 2*, both voltages and currents may be considered in order to provide additional mechanically  
20           related information, such as pressure related information etc.

## Claims

1. A detector constructed from fabric having electrically  
conductive elements and configured to produce electrical outputs in response  
5 to mechanical interactions, wherein  
a detector is divided into a plurality of regions;  
each of said regions includes a first conducting plane and a second  
conducting plane; and  
a mechanical interaction results in conducting planes of at least one of  
10 said regions being brought closer together.
2. A detector according to claim 1, wherein at least one of said  
conducting planes is unique to a region and the co-operating conducting  
plane is shared with a plurality of regions.  
15
3. A detector according to claim 2, wherein a single co-operating  
conducting plane is shared with all of said regions.
4. A detector according to any of claims 1 to 3, wherein signals  
20 are derived independently from a plurality of regions by a time division  
multiplexing operation.
5. A detector according to any of claims 1 to 4, wherein at least  
one of said planes includes first portions and second portions, said first  
25 portions have a higher resistance than said second portions and said first  
higher resistance portions are more flexible than said second portions.
6. The detector according to claim 5, wherein said higher  
resistance portions are configured as flexible portions to facilitate rotational  
30 movement about similar portions in a co-operating conductive plane.



7. A detector according to claim 5 or claim 6, wherein said second portions are further supported by solid portions.

5 8. A detector according to claim 7, wherein said solid portions are constructed from rubber, silicon or plastics.

9. A detector according to any of claims 1 to 8, wherein a potential is applied across at least one of said planes to determine the position of the  
10 mechanical interaction, and a second electrical property is determined to identify additional properties of said mechanical interactions.

10. A detector according to claim 9, configured to measure current or resistance as said second electrical property.

15 11. A detector according to claim 9 or claim 10, configured to determine applied force, applied pressure, area of contact or orientation of an object as the additional property of said mechanical interactions.

20 12. A method of constructing a detector from fabric having electrically conductive elements and configured to produce electrical outputs in response to mechanical interactions, comprising the steps of

dividing the detector into a plurality of regions;

25 providing a first conductive plane and a second conductive plane for each of said regions; and

bringing together conductive planes of at least one of said regions in a response to a mechanical interaction.

30 13. A method of constructing a detector according to claim 12, wherein at least one of said conducting planes is unique to a region and the

co-operating conducting plane is shared with a plurality of regions.

14. A method according to claim 13, wherein a single co-operating conducting plane is shared with all of said regions.

5

15. A method according to any of claims 12 to 14, wherein signals are derived independently from a plurality of regions by a time division multiplexing operation.

10

16. A method according to any of claims 12 to 15, wherein at least one of said planes includes first portions and second portions, said portions have a higher resistance than said second portions and said first higher resistance portions are more flexible than said second portions.

15

17. A method according to claim 16, wherein said higher resistance portions are configured as flexible portions to facilitate rotational movement about similar portions in a co-operating conductive plane.

20

18. A method according to claim 16 or claim 17, wherein said second portions are further supported by solid portions.

19. A method according to claim 18, wherein said solid portions are constructed from rubber, silicon or plastics.

25

20. A method according to any of claims 12 to 19, wherein a potential is applied across at least one of said planes to determine the position of the mechanical interaction, and a second electrical property is determined to identify additional properties of said mechanical interactions.

21. A detector constructed from fabric substantially as herein described with reference to *Figures 15, 16 and 17.*

22. A method of constructing a detector from fabric, substantially as  
5 herein described with reference to *Figures 15, 16 and 17.*



Application No: GB 9921923.0  
Claims searched: All

Examiner: Mark A Pullen  
Date of search: 20 January 2000

**Patents Act 1977**  
**Search Report under Section 17**

**Databases searched:**

UK Patent Office collections, including GB, EP, WO & US patent specifications, in:

UK CI (Ed.R): G1N (NACH, NACNR, NAEPR, NAFD8, NAGB8, NAGBR, NAQB),  
H1N (NBH, NUJD)

Int CI (Ed.7): G01L 1/20, G06K 11/12, 11/16

Other: ONLINE : WPI, EPODOC, JAPIO

**Documents considered to be relevant:**

Category	Identity of document and relevant passage	Relevant to claims
X,Y	GB 1308575 (DATA APPLIANCE) see page 2 lines 17-89	X:1-3, 12-14 Y:4,15
Y	US 4963703 (PHILLIPS et al) see all Figures	4,15

X	Document indicating lack of novelty or inventive step	A	Document indicating technological background and/or state of the art.
Y	Document indicating lack of inventive step if combined with one or more other documents of same category.	P	Document published on or after the declared priority date but before the filing date of this invention.
&	Member of the same patent family	E	Patent document published on or after, but with priority date earlier than, the filing date of this application.

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(52) UK CL (Edition R )

G1N NAQB N1A3B N1D9 N7H2 N7S

H1N NBH NUJD N449 N618 N705 N707 N744 N854

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NAGBR NAGB8 NAQB , H1N NBH NUJD

INT CL<sup>7</sup> G01L 1/20 , G06K 11/12 11/16

ONLINE : WPI, EPODOC, JAPIO

(54) Abstract Title

**Position detector constructed from conductive fabric**

(57) A position detector incorporates regions 1501-7 having first and second planes of conductive fabric, wherein a mechanical interaction brings the planes of at least one of the regions closer together. The fabric may be woven, knitted or non-woven eg felt. Preferably one of the planes is unique to a region and the other is shared by some or all of the regions. A potential difference applied across at least one of the planes can be used to determine the position of the mechanical interaction. Electrical signals can be derived independently from the regions by Time Division Multiplexing TMD (Fig. 3) via a microcontroller (201, Fig. 2) operated circuit (121, Fig. 2). At least one of the planes may consist of first and second portions (1206, 1205, Figs. 12A, 12B), the first portion having a higher resistance and being more flexible to allow complex curvature (Fig. 12B). Plates (1208, Figs. 12A, 12B) provide additional rigidity to the second portion. A second electrical property eg current or resistance can be used to identify additional properties of the mechanical interaction eg applied force, area of contact or orientation of an object.

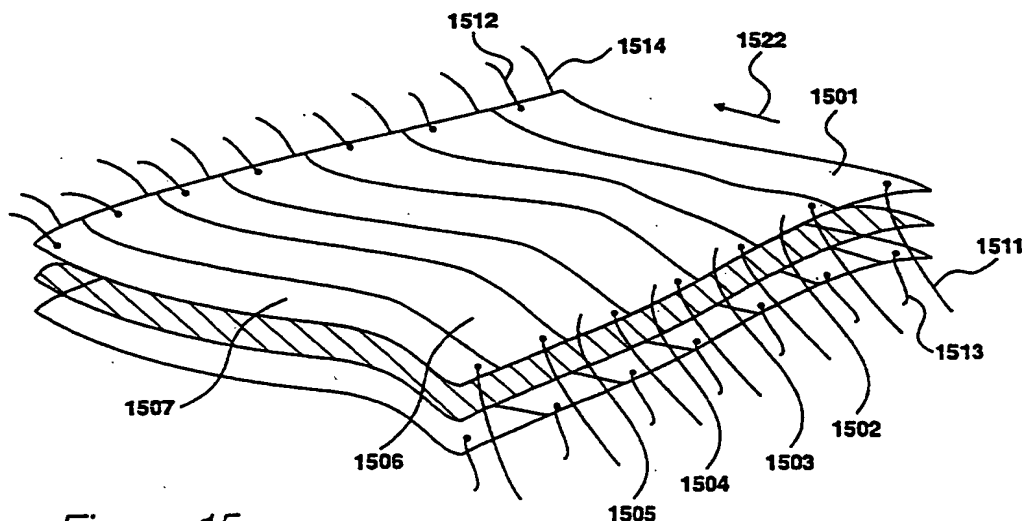


Figure 15

GB 2 341 932 A

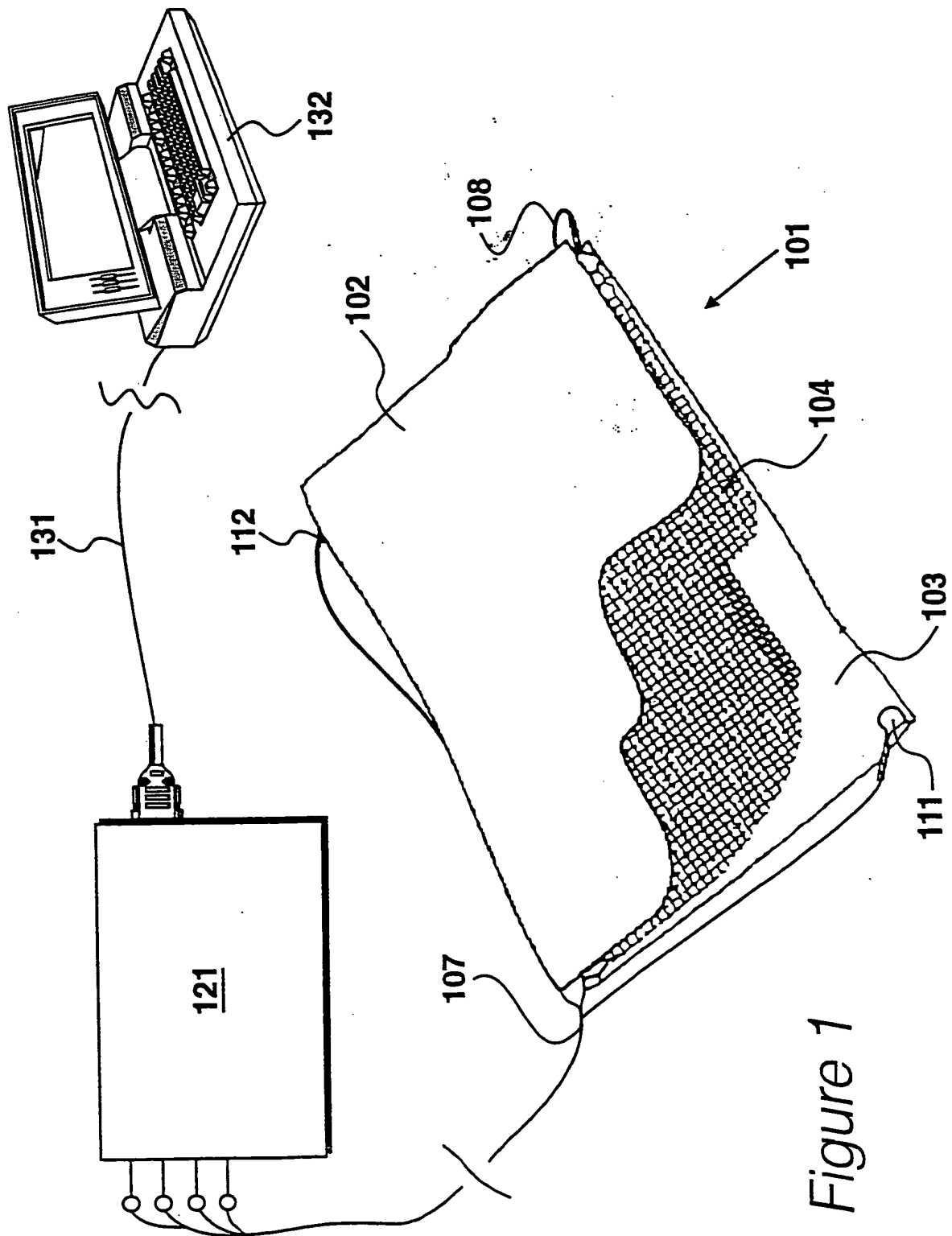


Figure 1

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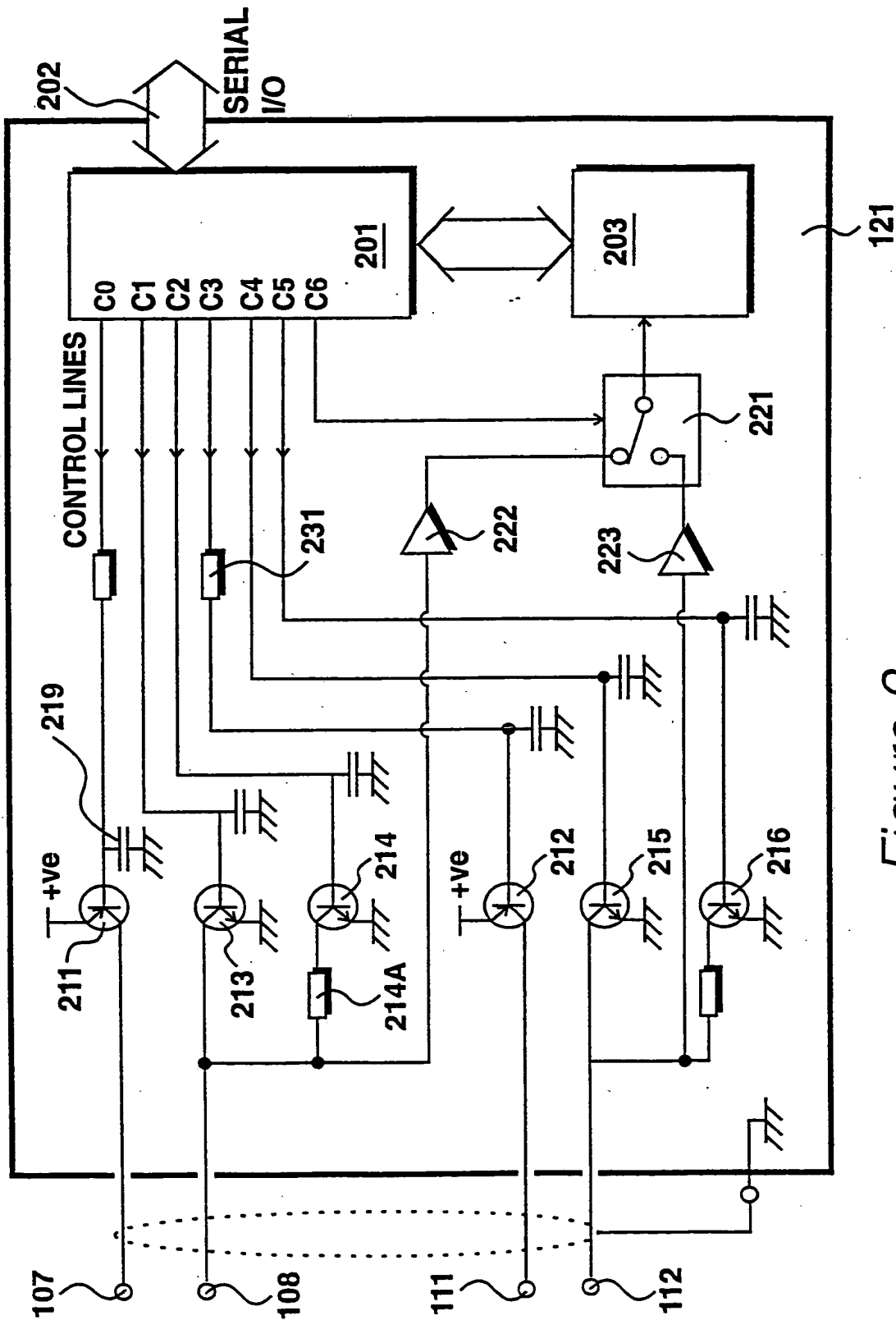
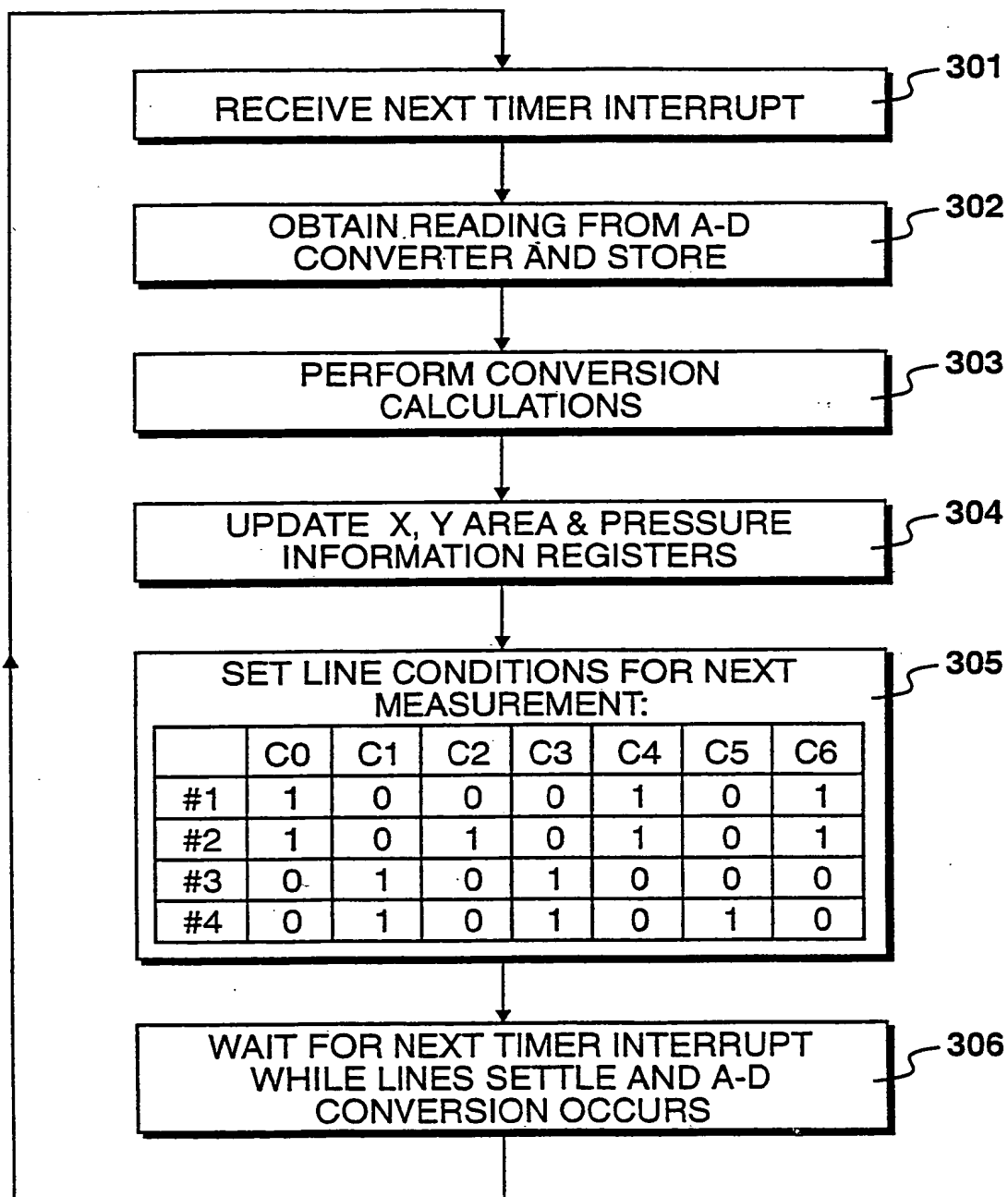


Figure 2

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*Figure 3*



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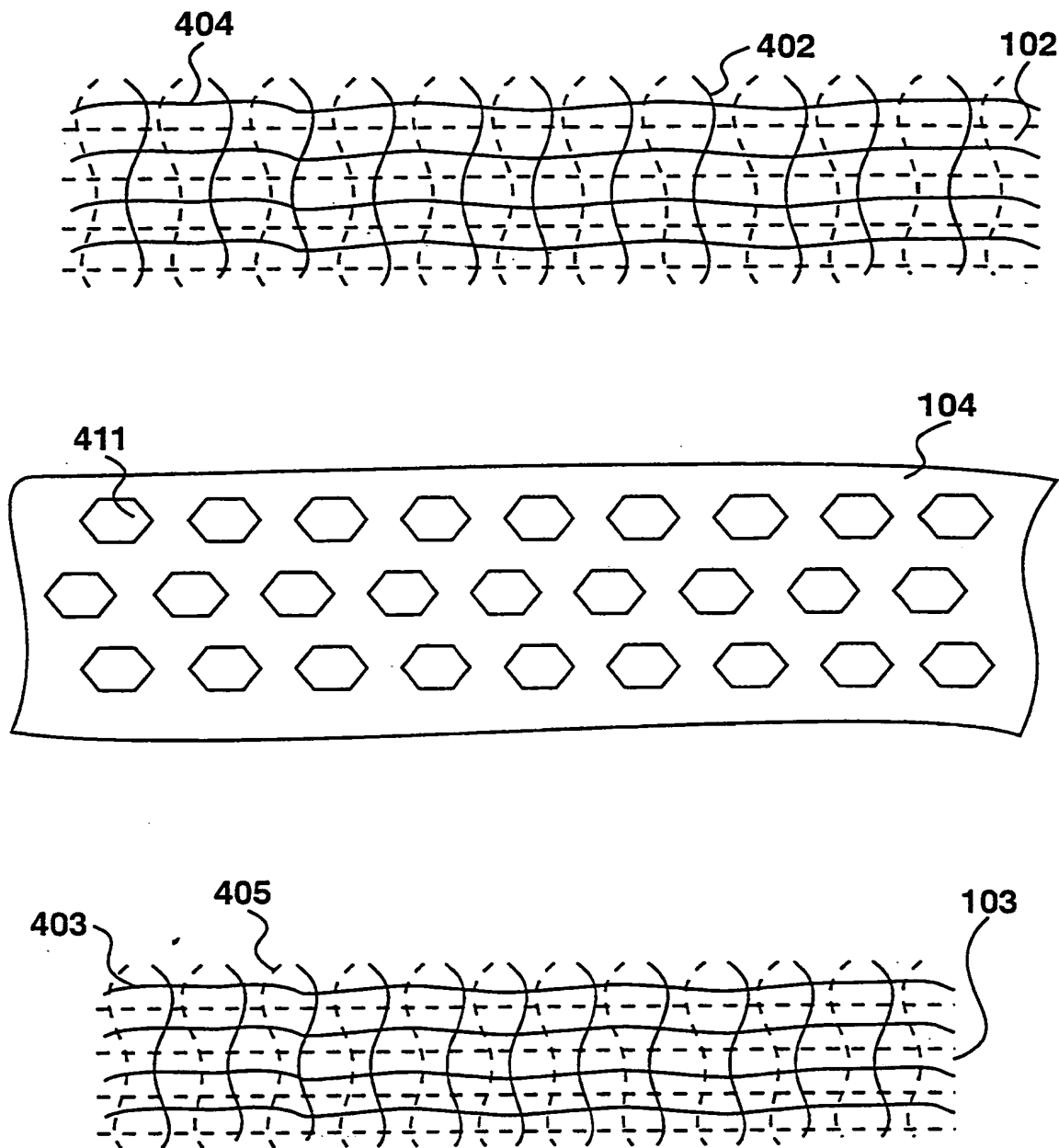
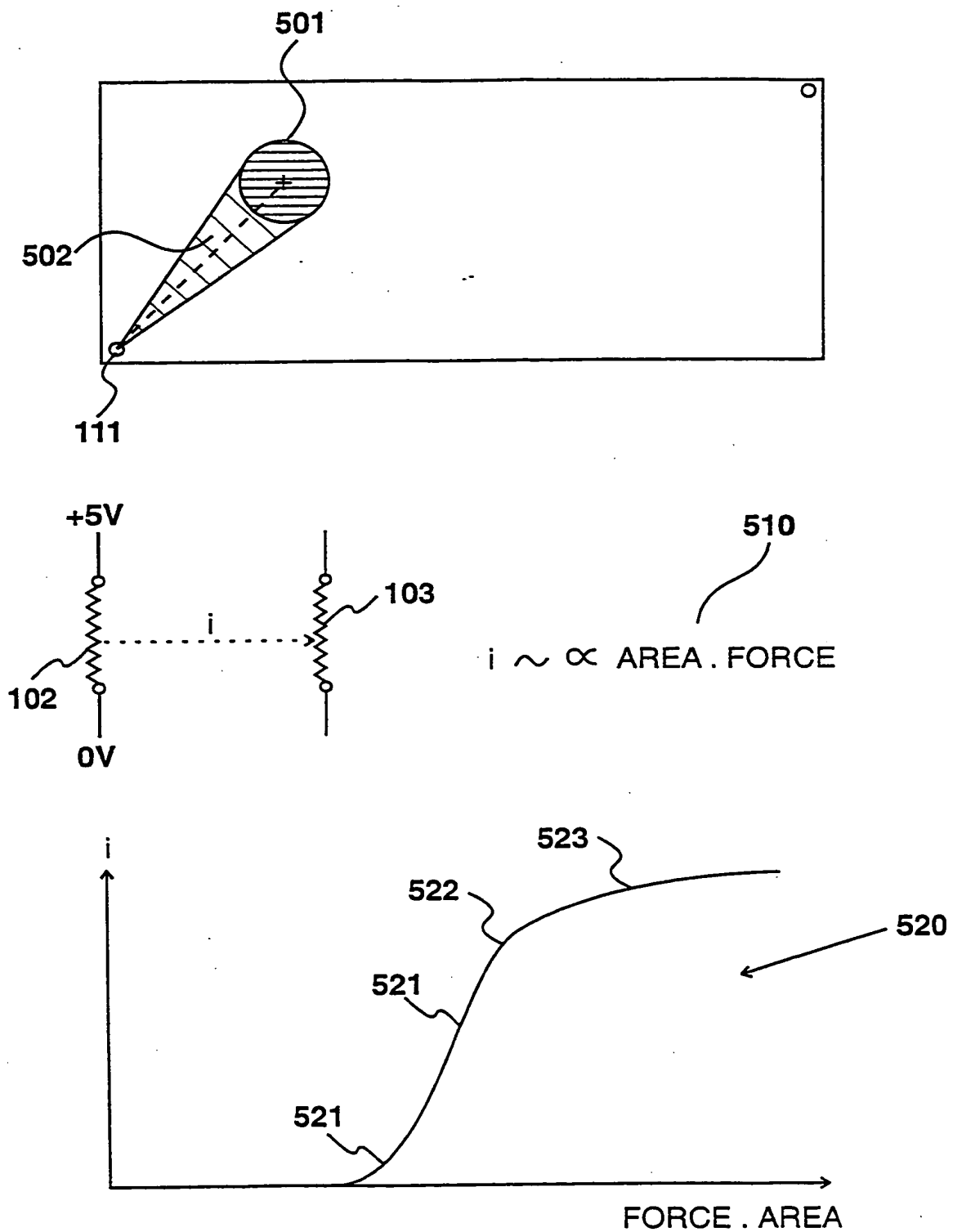


Figure 4

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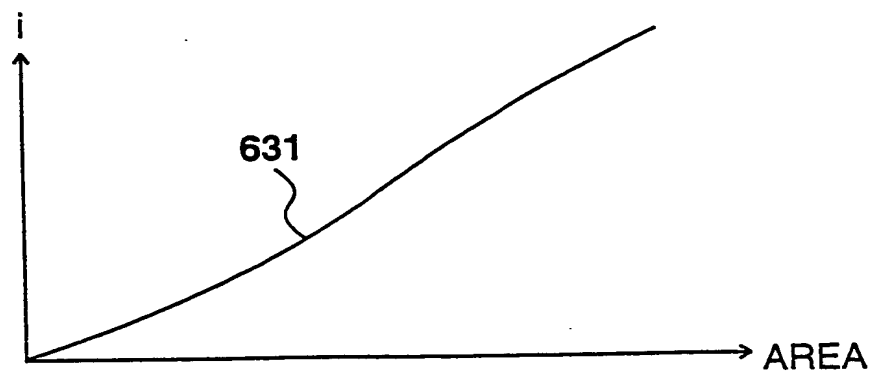
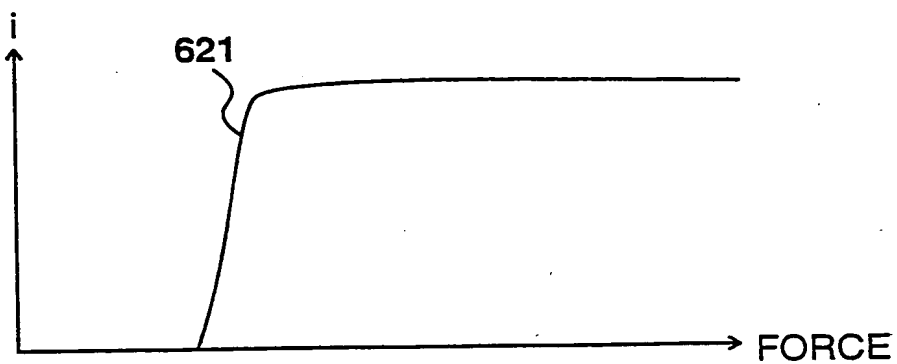
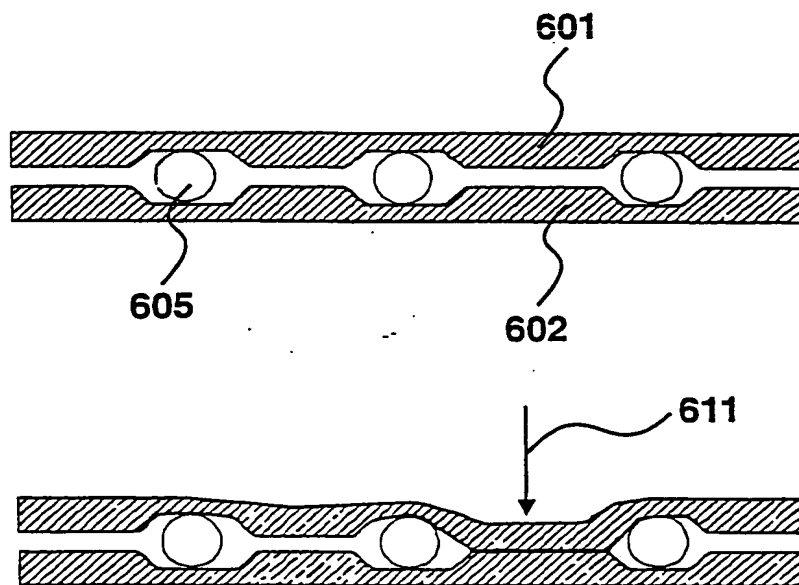


Figure 6

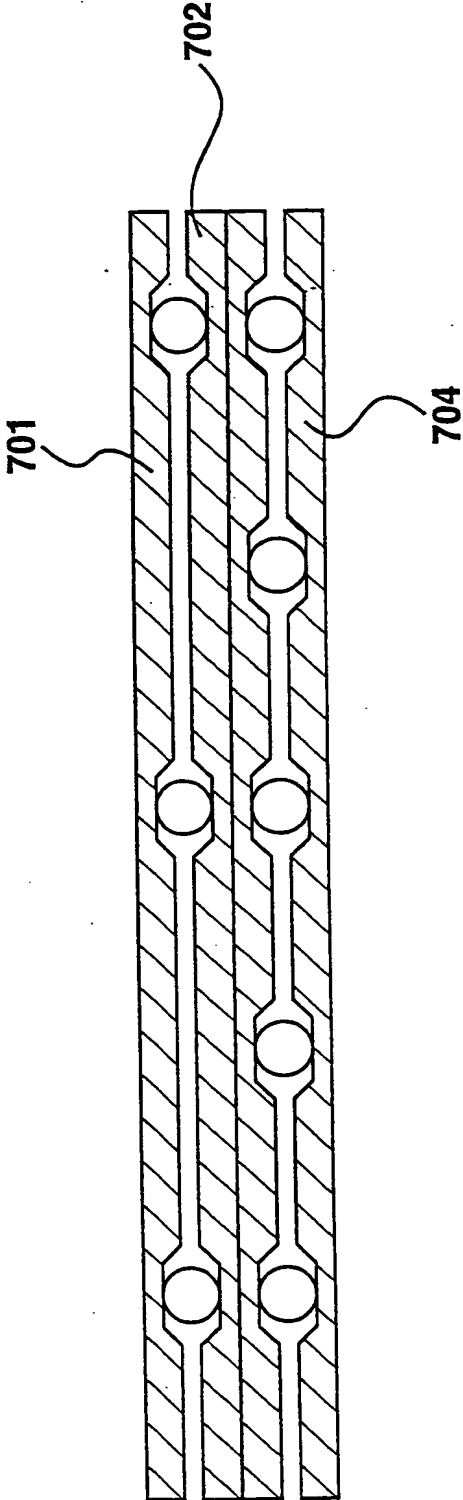


Figure 7

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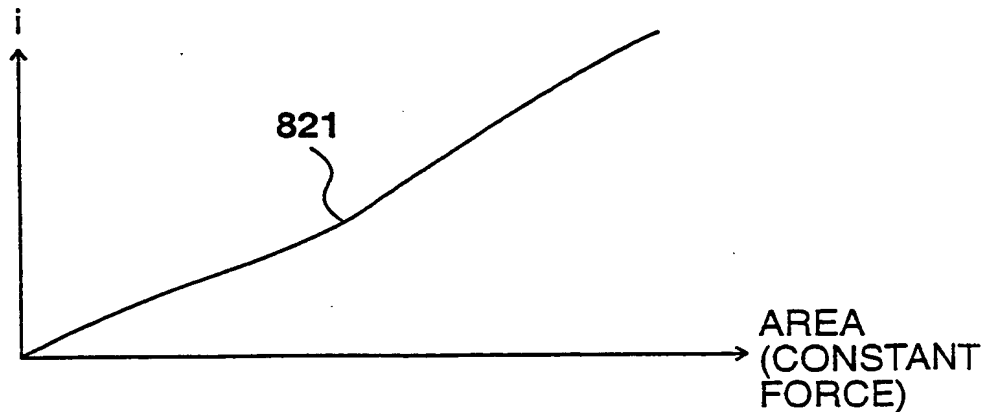
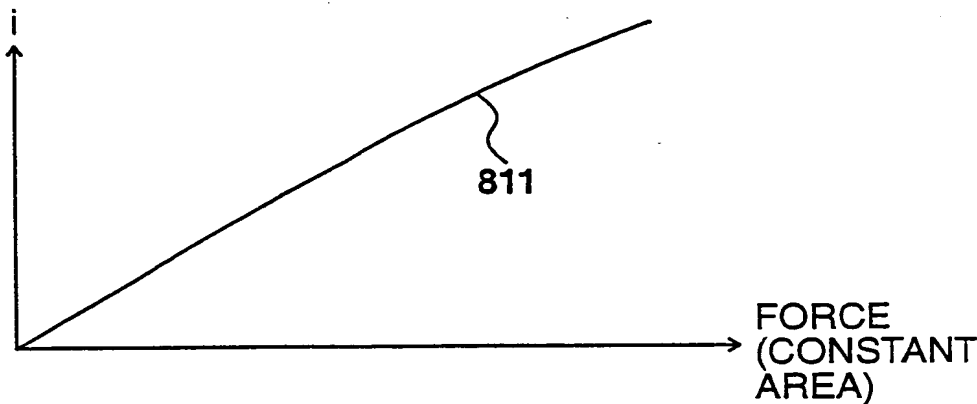
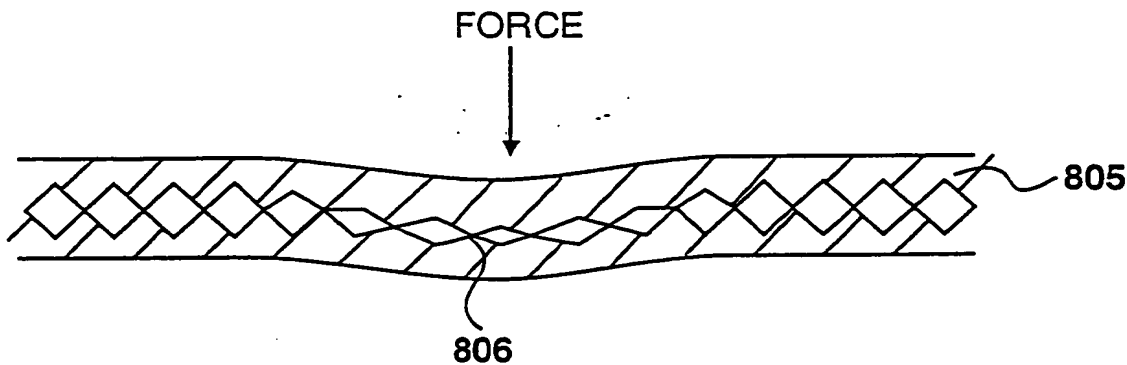
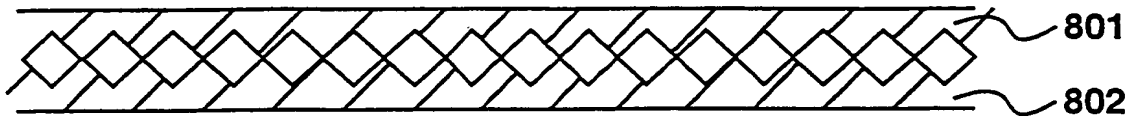
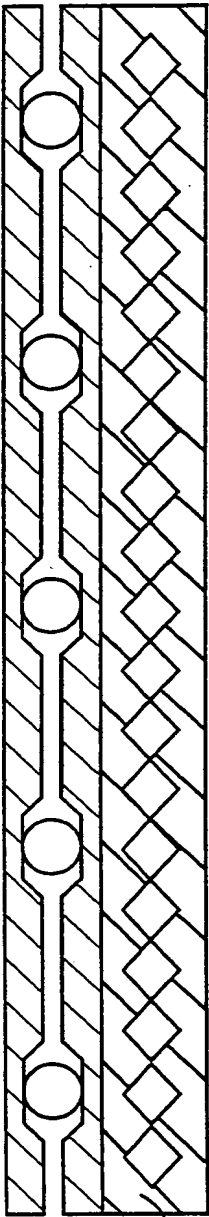


Figure 8



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Figure 9

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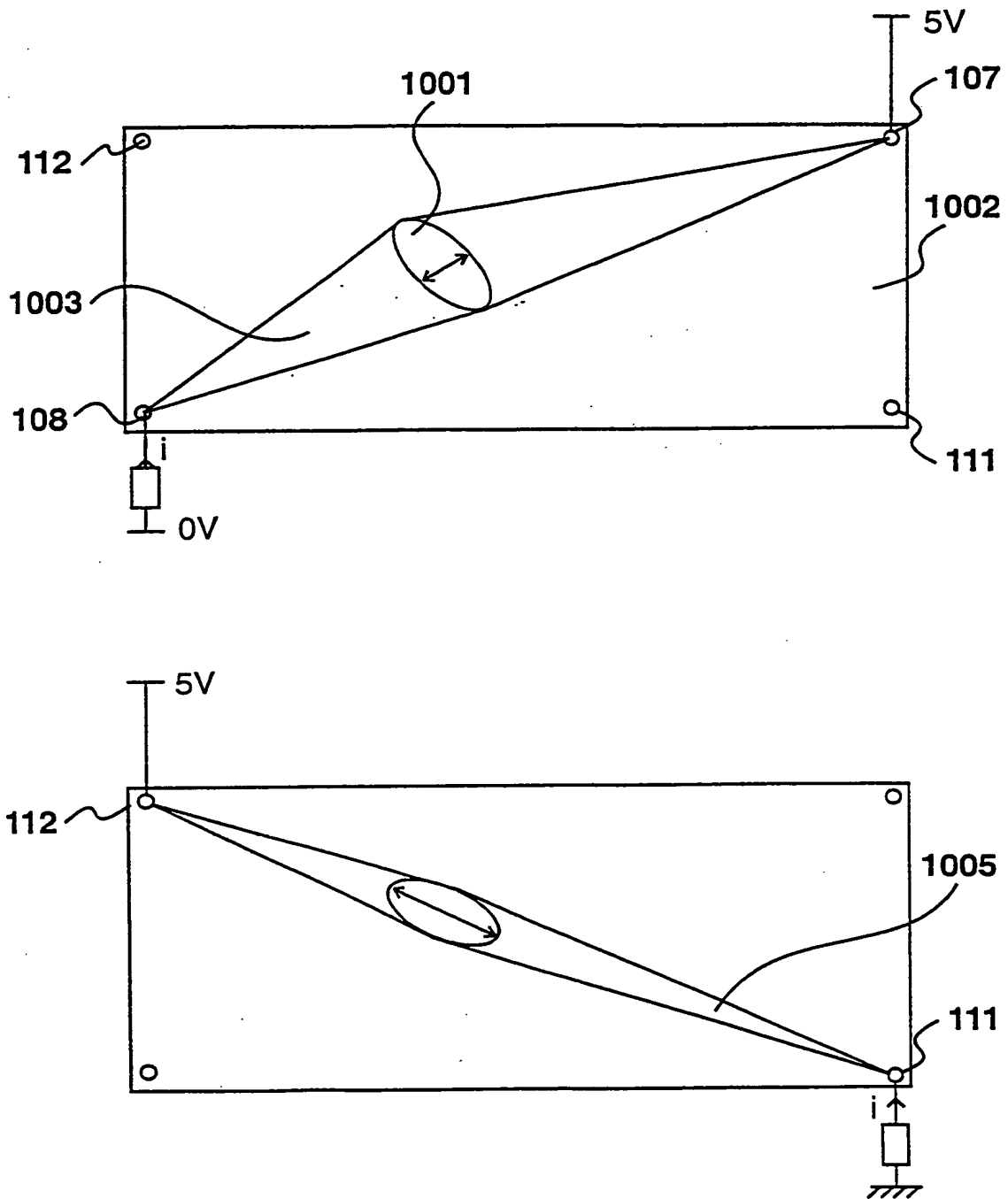
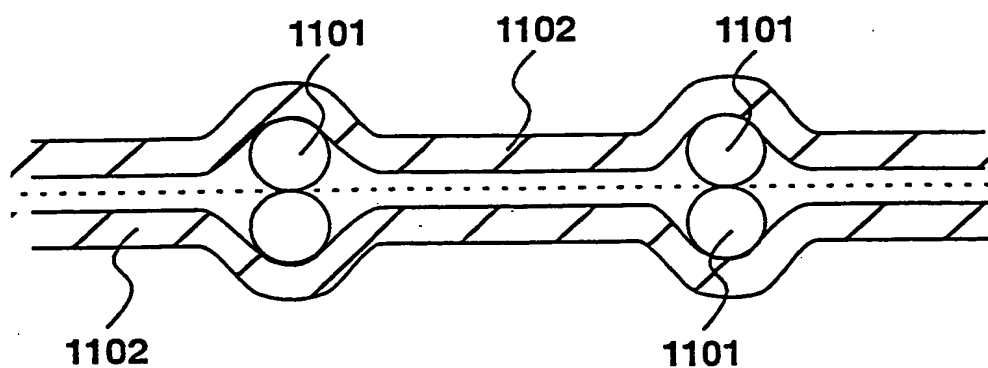
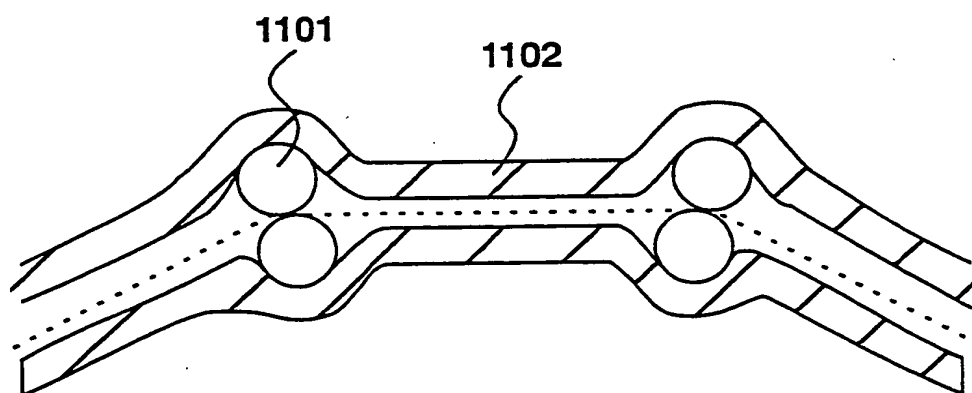


Figure 10

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*Figure 11A*



*Figure 11B*



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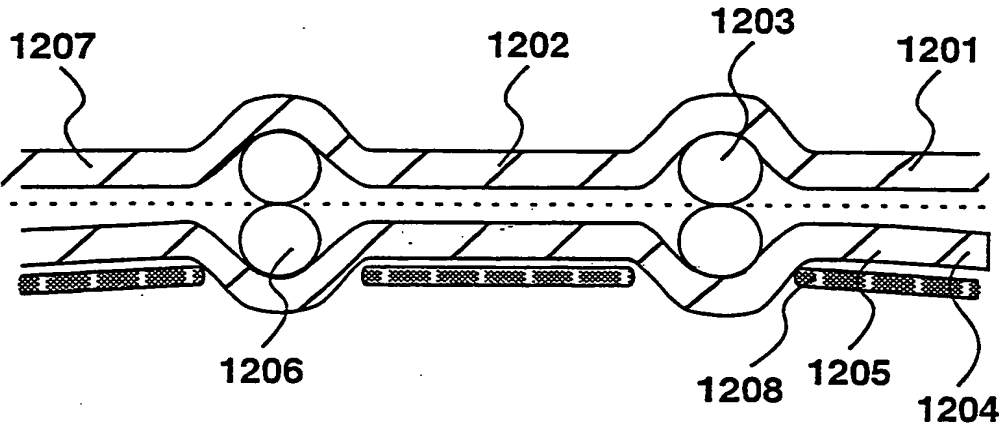


Figure 12A

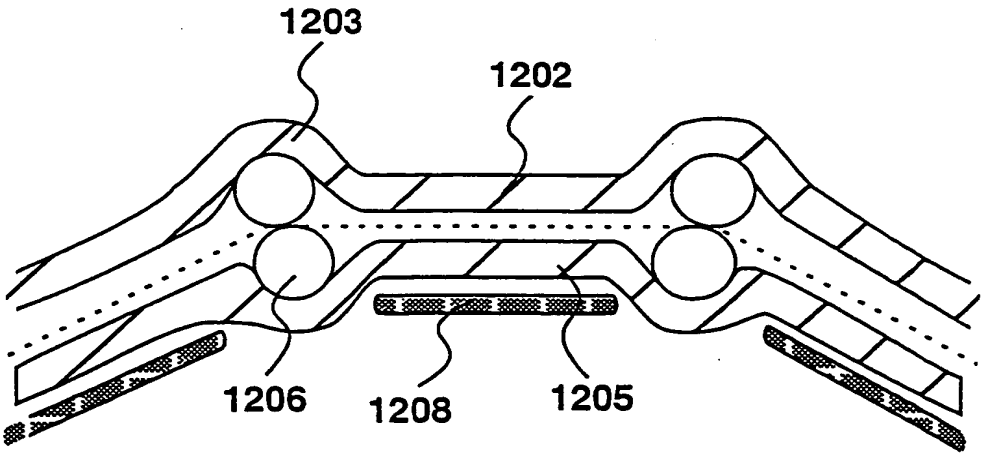


Figure 12B

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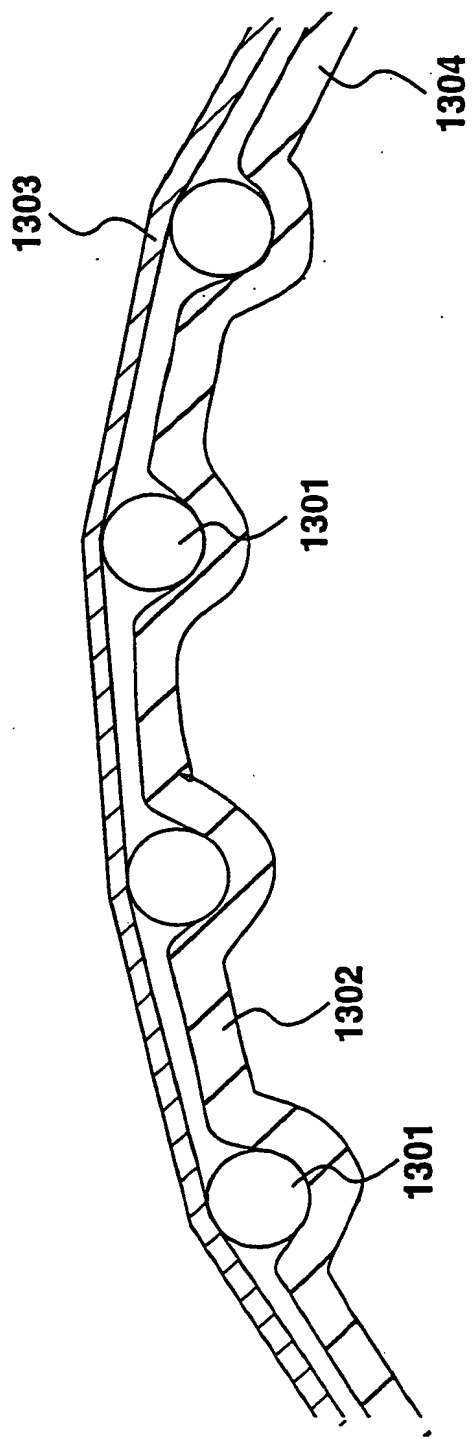


Figure 13

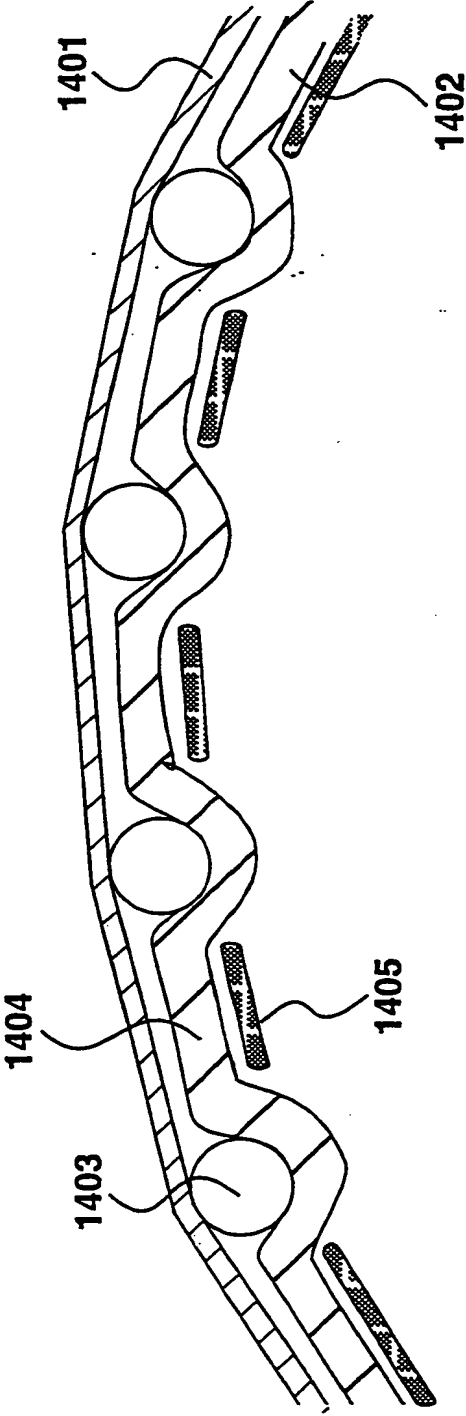


Figure 14

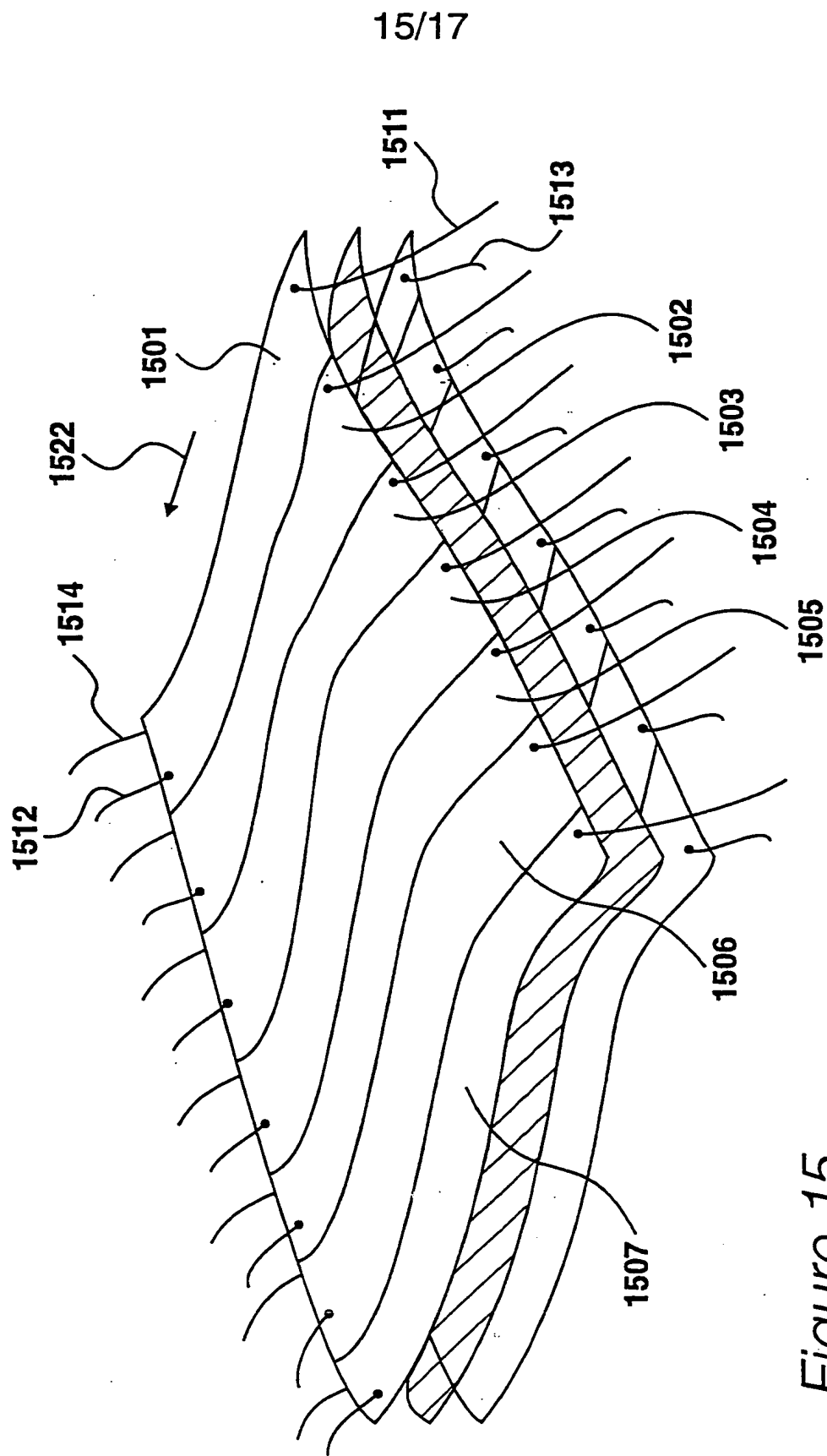


Figure 15

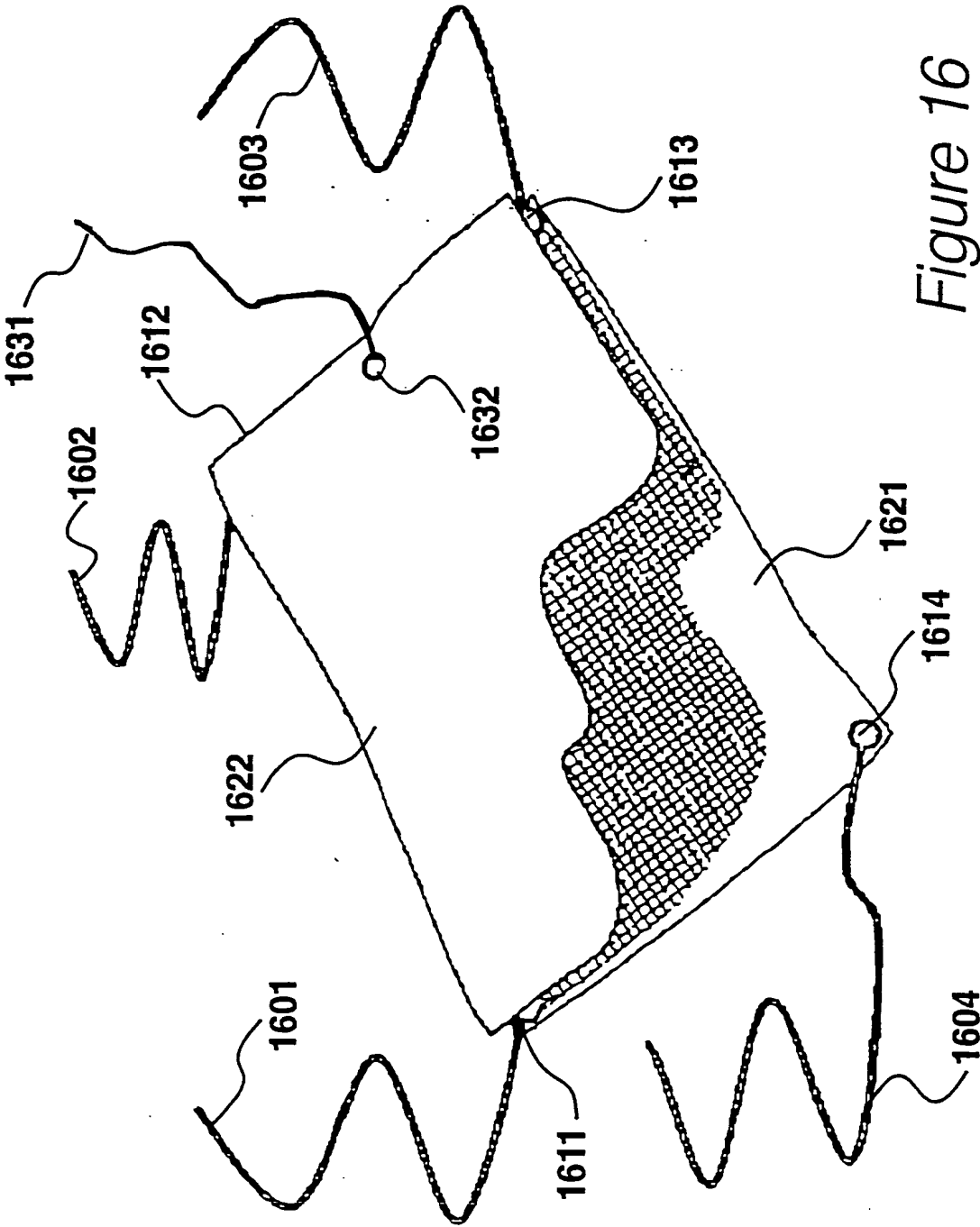


Figure 16

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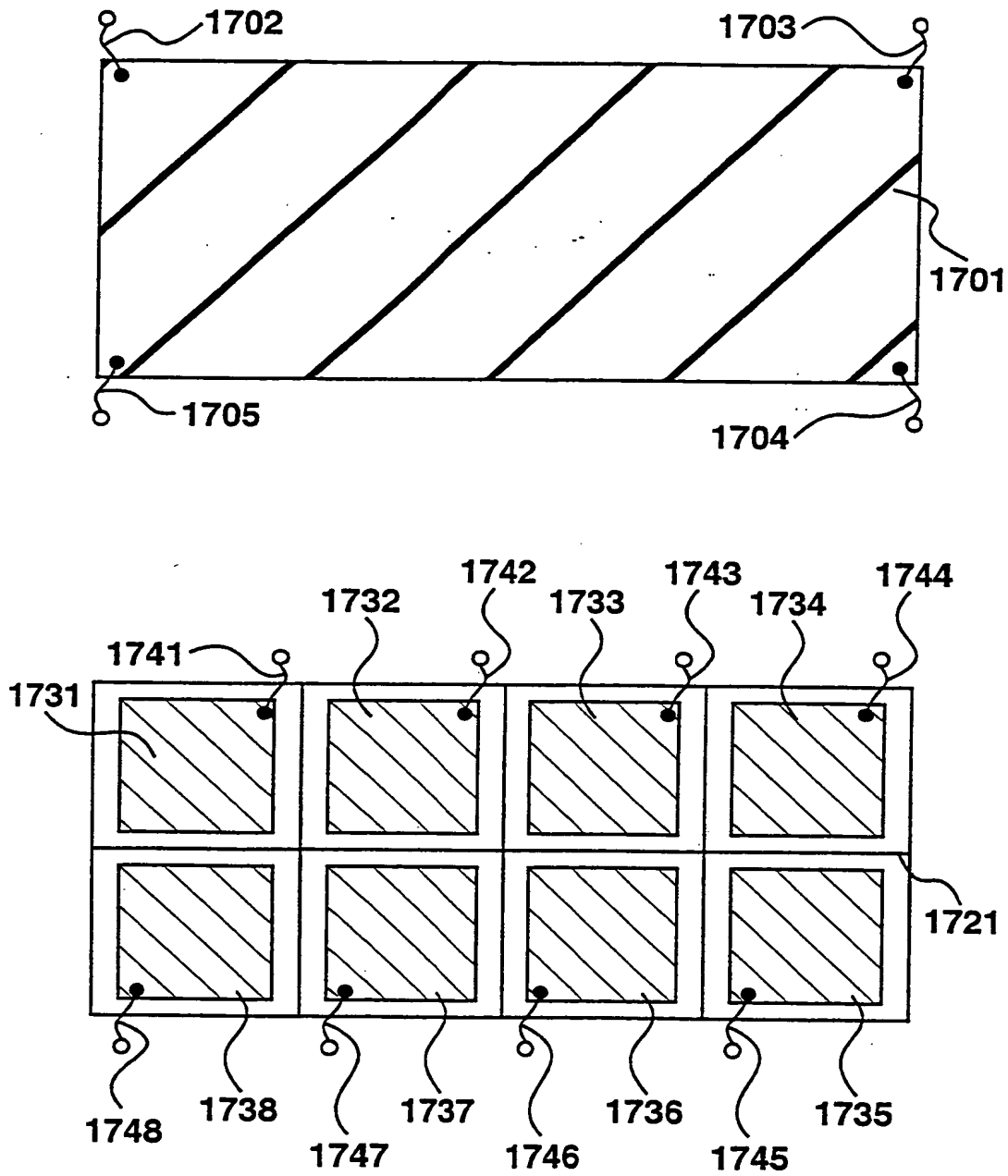


Figure 17

## Detector Constructed From Fabric

5 The present invention relates to a detector constructed from fabric having electrically conductive elements and configured to produce electrical outputs in response to mechanical interactions.

A fabric touch sensor for providing positional information is described in United States Patent 4,659,873 of Gibson. The sensor is fabricated using two layers of fabric having conducting threads, separated by a resistive layer to prevent unintentional contact.

10 An improvement to this proposal is disclosed in the applicant's co-pending British patent application number 98 20 902 in which there is provided a position detector constructed from fabric having electrically conductive elements, comprising at least two electrically conductive planes. A potential is applied across at least one of the planes to determine the position  
15 of a mechanical interaction. In addition, a second electrical property is determined, such as current, to identify additional properties to the mechanical interaction, such as an applied force, an applied pressure or an area of contact.

20 A further improvement is disclosed in the applicant's co-pending British patent application number 98 20 905, in which there is provided a detector constructed from fabric having electrically conductive elements to define at least two electrically conductive planes and configured to produce an electrical output in response to a mechanical interaction. At least one of the planes includes first portions and second portions, wherein the said first  
25 portions have a higher resistance than the second portions and the first higher resistance portions are more flexible than the second portions.

The second improvement provides the advantage of facilitating a folding or distortion of the detector whilst still maintaining full functionality.

## Detector Constructed From Fabric

The present invention relates to a detector constructed from fabric having electrically conductive elements and configured to produce electrical outputs in response to mechanical interactions.

A fabric touch sensor for providing positional information is described in United States Patent 4,659,873 of Gibson. The sensor is fabricated using two layers of fabric having conducting threads, separated by a resistive layer to prevent unintentional contact.

An improvement to this proposal is disclosed in the applicant's co-pending British patent application number 98 20 902 in which there is provided a position detector constructed from fabric having electrically conductive elements, comprising at least two electrically conductive planes. A potential is applied across at least one of the planes to determine the position of a mechanical interaction. In addition, a second electrical property is determined, such as current, to identify additional properties to the mechanical interaction, such as an applied force, an applied pressure or an area of contact.

A further improvement is disclosed in the applicant's co-pending British patent application number 98 20 905, in which there is provided a detector constructed from fabric having electrically conductive elements to define at least two electrically conductive planes and configured to produce an electrical output in response to a mechanical interaction. At least one of the planes includes first portions and second portions, wherein the said first portions have a higher resistance than the second portions and the first higher resistance portions are more flexible than the second portions.

The second improvement provides the advantage of facilitating a folding or distortion of the detector whilst still maintaining full functionality.



According to a first aspect of the present invention, there is provided a detector constructed from fabric having electrically conductive elements and configured to produce electrical outputs in response to mechanical interactions, wherein a detector is divided into a plurality of regions; each of said regions includes a first conducting plane and a second conducting plane; and a mechanical interaction results in conducting planes of at least one of said regions being brought closer together.

In a preferred embodiment, one of said conducting planes is unique to a region and the co-operating conducting plane is shared with a plurality of regions. A single co-operating conducting plane may be shared with all of the regions.

Preferably, signals are derived independently from a plurality of regions by a time division multiplexing operation.

According to a second aspect of the present invention, there is provided a method of constructing a detector from fabric having electrically conductive elements and configured to produce electrical outputs in response to mechanical interactions, comprising the steps of dividing the detector into a plurality of regions; providing a first conductive plane and a second conductive plane for each of said regions; and bringing together conductive planes of at least one of said regions in response to a mechanical interaction.

The invention will be described by way of example only, with reference to the accompanying drawings of which:

*Figure 1* shows a position detector constructed from fabric;

*Figure 2* shows a control circuit identified in *Figure 1*;

*Figure 3* details operations performed by the micro-controller identified in *Figure 2*;

*Figure 4* details planes identified in *Figure 1*;

*Figure 5* details current flow due to mechanical interaction;

*Figure 6* details an alternative construction for conducting fabric planes;

*Figure 7* shows an alternative configuration of conducting planes;  
*Figure 8* shows an alternative configuration of conducting planes;  
*Figure 9* details a composite configuration of conducting planes; and  
*Figure 10* shows an asymmetric object interacting with conducting  
5 planes.

*Figure 11A* and *Figure 11B* show an alternative construction for a  
detector;

*Figure 12A* and *Figure 12B* show a further alternative construction;

*Figure 13* shows a further alternative construction;

10 *Figure 14* shows a further alternative construction.

*Figure 15* shows an alternative embodiment having a plurality of  
detectors;

*Figure 16* shows an alternative detector configuration; and

*Figure 17* shows multiple detectors of the type shown in *Figure 16*.

15 A position detector **101** constructed from fabric is shown in *Figure 1*.  
The detector has two electrically conducting fabric planes, in the form of a  
first plane **102** and a second plane **103**. The planes are separated from each  
other and thereby electrically insulated from each other, by means of an  
insulating mesh **104**. When force is applied to one of the planes, the two  
20 conducting planes are brought together, through the mesh **104**, thereby  
creating a position at which electrical current may conduct between planes  
**102** and **103**. In this way, it is possible to identify the occurrence and/or  
position of a mechanical interaction.

25 The fabric planes are defined by fabric structures, which may be  
considered as a woven, non-woven (felted) or knitted etc. The fabric layers  
may be manufactured separately and then combined to form the detector or  
the composite may be created as part of the mechanical construction  
process.

30 When a voltage is applied across terminals **107** and **108**, a voltage  
gradient appears over plane **102**. When a mechanical interaction takes place,

plane 103 is brought into electrical contact with plane 102 and the actual voltage applied to plane 103 will depend upon the position of the interaction. Similarly when a voltage is applied between connectors 111 and 112, a voltage gradient will appear across plane 103 and mechanical interaction will result in a voltage being applied to plane 102. Similarly, the actual voltage applied to plane 102 will depend upon the actual position of the interaction. In this way, for a particular mechanical interaction, it is possible to identify locations within the plane with reference to the two aforesaid measurements. Thus, connectors 107, 108, 111 and 112 are received by a control circuit 121, configured to apply voltage potentials to the detector 101 and to make measurements of electrical properties in response to mechanical interactions.

Control circuit 121 identifies electrical characteristics of the sensor 101 and in response to these calculations, data relating to the characteristics of the environment are supplied to a data processing system, such as a portable computer 131, via a conventional serial interface 131.

Control circuit 121 is detailed in *Figure 2*. The control circuit includes a micro-controller 201 such as a Philips 80C51 running at a clock frequency of twenty megahertz. Operations performed by micro-controller 201 are effected in response to internally stored commands held by an internal two kilobyte read-only memory. The micro-controller also includes one hundred and twenty-eight bytes of randomly accessible memory to facilitate intermediate storage while performing calculations. Micro-controller 201 includes a serial interface 202 in addition to assignable pins and an interface for communicating with an analogue to digital converter 203, arranged to convert input voltages into digital signals processable by the micro-controller 201.

The control circuit 121 includes two PNP transistors 211 and 212, in addition to four NPN transistors 213, 214, 215 and 216. All of the transistors are of relatively general purpose construction and control switching operations within the control circuit so as to control the application of voltages to the position detector 101.

In operation, measurements are made while a voltage is applied across first plane **102** and then additional measurements are made while a voltage is applied across the second plane **103**; and output voltage only being applied to one of the planes at any particular time. When an output voltage is applied to one of the planes, plane **102** or plane **103**, input signals are received from the co-operating plane **103** or **102** respectively. Input signals are received by the analogue to digital converter **203** via a selection switch **221**, implemented as a CMOS switch, in response to a control signal received from pin C6 of the micro-controller **201**. Thus, in its orientation shown in *Figure 2*, switch **221** has been placed in a condition to receive an output from a first high impedance buffer **222**, buffering an input signal received from plane **102**. Similarly, when switch **221** is placed in its alternative condition, an input is received from a second high impedance buffer **223**, configured to receive an input signal from plane **103**. By placing buffers **222** and **223** on the input side of CMOS switch **221**, the switch is isolated from high voltage electrostatic discharges which may be generated in many conditions where the detector undergoes mechanical interactions.

In the condition shown in *Figure 2*, switch **221** is placed in its upper condition, receiving input signals from buffer **222**, with output signals being supplied to the second plane **103**. Further operation will be described with respect to this mode of operation and it should be appreciated that the roles of the transistor circuitry is reversed when switch **221** is placed in its alternative condition. As previously stated, condition selection is determined by an output signal from pin C6 of micro-controller **201**. In its present condition the output from pin C6 is low and switch **221** is placed in its alternative configuration when the output from pin 6 is high.

Output pin C0 controls the conductivity of transistor **211** with pins C1 to C5 having similar conductivity control upon transistors **212**, **213**, **214**, **215** and **216** respectively.

Transistors **211** and **213** are switched on when a voltage is being applied to the first plane **102** and are switched off when a voltage is being applied to the second plane **103**. Similarly, when a voltage is being applied to the second plane **103**, transistors **212** and **215** are switched on with transistors **211** and **213** being switched off. In the configuration shown in *Figure 2*, with switch **221** receiving an input from buffer **222**, output transistors **211** and **213** are switched off with output transistors **212** and **215** being switched on. This is achieved by output pin C0 being placed in a high condition and pin C1 being placed in a low condition. Similarly, pin C3 is placed in a low condition and pin C4 is placed in a high condition.

In the configuration shown, C3 is placed in a low condition, as previously described. The micro-controller **201** includes a pull-down transistor arranged to sink current from the base of transistor **212**, resulting in transistor **212** being switched on to saturation. Consequently, transistor **212** appears as having a very low resistance, thereby placing terminal **111** at the supply voltage of five volts. Resistor **231** (4K7) limits the flow of current out of the micro-controller **201**, thereby preventing burn-out of the micro-controller's output transistor.

Pin C4 is placed in a high state, resulting in transistor **215** being placed in a conducting condition. A serial resistor is not required given that the micro-controller **201** includes internal pull-up resistors, as distinct from a pull-up transistor, such that current flow is restricted. Thus, transistors **212** and **215** are both rendered conductive, resulting in terminal **111** being placed at the positive supply rail voltage and terminal **112** being placed at ground voltage. The capacitors shown in the circuit, such as capacitor **219**, limit the rate of transistor transitions thereby reducing rf transmissions from the sensor **101**.

With transistors **212** and **215** placed in their conductive condition, input signals are received from the first plane **102** in the form of a voltage applied to terminal **108**. For position detection, this voltage is measured

directly and transistor **214** is placed in a non-conductive condition by output pin C2 being placed in a low condition. Under these conditions, the voltage from input terminal **108** is applied to analogue to digital converter **203** via buffer **222** and switch **221**.

5           In accordance with the present invention, a second electrical property is determined which, in this embodiment, represents the current flowing through the sensor in response to a mechanical interaction. The current measurement is made by placing transistor **215** in a conductive condition, by placing output pin C4 in a high condition. In this condition, current received at  
10       terminal **108** is supplied to transistor **214** via resistor **214A**, having a resistance of typically 5k selectable so as to correspond to the characteristics of the sensor. A voltage is supplied to A to D converter **203** via buffer **222** and switch **221** but on this occasion the voltage represents a voltage drop, and hence a current, across resistor **214A**.

15           Thus, transistors **212** and **215** are placed in a conducting condition, transistor **214** is placed in a non-conducting condition, so as to measure voltage, and is then placed in a conducting condition so as to measure current. The roles of the transistors are then reversed, such that output transistors **211** and **213** are placed in a conducting condition, with transistors  
20       **212** and **215** being placed in a non-conducting condition (and switch **221** reversed) allowing a voltage to be measured by placing transistor **216** in a non-conducting condition, and then allowing a current to be measured by placing transistor **216** in a conducting condition.

25           The cycling of line conditions, in order to make the measurements identified previously, is controlled by a clock resident within micro-controller **201**. After each condition has been set up, a twelve bit number is received from the digital to analogue converter **203** and this number is retained within a respective register within micro-controller **201**. Thus, after completing a cycle of four measurements, four twelve bit values are stored within the  
30       micro-controller **201** for interrogation by the processing device **131**.

Furthermore, the rate of cycling may be controlled in response to instructions received from the processing device 131.

Operations performed by micro-controller 201 are detailed in *Figure 3*. The micro-controller continually cycles between its four configuration states and each time a new input is produced, representing a current or a voltage in one of the two configurations, new output data is calculated on an on-going basis. Thus, output registers are updated such that the best data is made available if the micro-controller is interrupted by the external processor 131.

The micro-controller 201 is fully interrupt driven in terms of receiving external interrupts for data interrogation along with internal interrupts in order to initiate a configuration cycle. The external interrupt has a higher priority such that external processor 131 is provided with information as soon as possible in response to making an interrupt request.

Internally interrupts for the micro-controller 201 are generated by its own internal timer and the procedure shown in *Figure 3* is effectively held in a wait state until a next timer interrupt is received at step 301. The wait state allows voltage levels on connections 107, 108, 111 and 112 to become stable and provides sufficient time for valid data to be received from the analogue to digital converter 203.

At step 302, an output is received from analogue to digital converter 203 and at step 303 calculations are performed with respect to the most current data received from the analogue to digital converter, so as to convert numerical values relating to voltages and currents into numerical values representing properties of the mechanical interaction. Thus, after performing calculations at step 303, appropriate registers are updated at step 304 and it is these registers that are interrogated in response to an interrupt received from processing system 131.

At step 305 next conditions for the output lines are set by appropriate logic levels being established for output pins C0 to C6. After the next output condition has been selected, the processor enters a wait state at step 306,

allowing the electrical characteristics to settle, whereafter processing continues in response to the next timer interrupt.

Thus, it should be appreciated that on each iteration of the procedure shown in *Figure 3*, one of the output conditions is selected at step 305. Thus, it should be appreciated that the input data is effectively delayed and does not represent a condition of the electrical characteristics at an instant. If in practice, the delay between measurements becomes too large, it becomes necessary to enhance the frequency of operation of circuits within the control system shown in *Figure 2*. Thus, the rate of conversion for converter 203 would need to be increased and the circuitry would need to be redesigned for high frequency operation. This in turn could create problems in terms of high frequency interference resulting in enhanced shielding being required for the facility as a whole.

When output condition number one is selected, an output voltage at 108 is determined. On the next cycle, identified as output condition number two, the current flowing through connector 108 is determined. On the next iteration, under output configuration number three, the voltage appearing at connector 112 is determined and on the next cycle, identified as condition number four, the current flowing through connector 112 is determined. After each of these individual measurements, new data is generated in response to steps 303 and 304 such that resulting output registers are being regularly updated on a continual basis, such that the processing system 131 may effectively perform a continual monitoring operation in terms of changes made to the mechanical interactions with the detector 101.

In a typical implementation, the four characteristic measurements, making up a complete cycle, will be repeated at a frequency of between twenty-five to fifty times per second. In situations where such a repetition rate is not required, it may be preferable to increase the duration of the wait states and thereby significantly reduce overall power consumption.



Planes 102, 103 and 104 of the detector 101 are detailed in *Figure 4*. Planes 101 and 103 are of substantially similar construction and are constructed from fabric having electrically conductive elements 402 in plane 102 along with similar electrical conductive elements 403 in plane 103. Thus, it is possible for a voltage indicative of position to be determined when conductive elements 402 are placed in physical contact with conductive elements 403.

The overall resistivity of planes 402 and 403 are controlled by the inclusion of non-conducting elements 404 and 405. Thus, resistivity is controlled by controlling the relative quantities and/or densities of conductive elements 402 with non-conductive elements 404. Resistivity may also be controlled by selecting an appropriate fibre type, adjusting the thickness of the fibre or adjusting the number of strands present in a yarn.

Plane 404 represents a non-conducting insulating spacer positioned between the two conducting planes 102 and 103. Plane 104 is constructed as a moulded or woven nylon sheet having an array of substantially hexagonal holes 411, the size of holes 411 is chosen so as to control the ease with which it is possible to bring conductive elements 402 into physical contact with conductive elements 403. Thus, if relatively small holes 411 are chosen, a greater force is required in order to bring the conductive elements together. Similarly, if the size of the hole is increased, less force is required in order to achieve the conductive effect. Thus, the size of holes 411 would be chosen so as to provide optimal operating conditions for a particular application. Operating conditions may also be adjusted by controlling the thickness of layer 104, its surface flexibility and the contour of co-operating planes 102 and 103.

When a potential is applied across one of the conducting planes, the actual potential detected at a point on that plane will be related to the position at which the measurement is made. Thus, a direct voltage measurement from the co-operating plane gives a value from which a positional co-ordinate

may be determined. By reversing the plurality of the planes and taking a measurement from the opposing plane, two co-ordinates are obtained from which it is then possible to identify a precise location over the planar surface.

In addition to measuring position on the planar surface, the present invention is directed at identifying additional electrical properties in order to determine properties of the mechanical interaction. As previously described, the system is configured to measure currents in addition to measuring voltages.

When the two conducting planes are brought into mechanical contact, due to a mechanical interaction, the amount of current flowing as a result of this contact will vary in dependence upon the actual position of the plane where the mechanical interaction takes place. The position of the mechanical interaction has also been determined with reference to voltages and it could be expected that these two quantities will vary in a substantially similar way, each representing the same physical situation. Experience has shown that variations in measured current do not follow exactly the same characteristic as variations in measured voltage. As illustrated in *Figure 5*, the amount of current flowing due to a mechanical interaction will depend upon the position of a mechanical interaction **501**. However, in addition to this, the amount of current flow will also depend upon the size of the mechanical interaction. As the size of the mechanical interaction increases, there is a greater area of contact and as such the overall resistance of the mechanical interaction is reduced. However, it should be appreciated that variations in terms of current with respect to interaction size is a sophisticated relationship, given that, in addition to the resistivity of the contact area **501**, the resistivity of the actual electrical connections within the sheet must also be taken into account.

Thus, current is transmitted through a region **502** in order to provide a current to the contact region **501**. Some aspects of this effect will be compensated with reference to position calculations and other variations due to this effect may be compensated by a non-linear analysis of the input data.

Contact area resistivity is illustrated generally at 510 and shows that the amount of current flowing between plane 102 and plane 103 is considered as being related to the area of mechanical interaction, which is related to the area of contact externally and to the level of externally applied mechanical force.

The resulting non-linear relationship between the force area product and the resulting current flow is illustrated generally at 520. At 521 there is an initial threshold point, identifying the point at which the gap starts to be closed, followed by an operational part of the curve which may give useful indications of pressure up to point 522, whereafter the relationship becomes very non-linear until position 523 where the relationship effectively saturates.

Using a detector of the type illustrated in *Figure 1*, it is possible to measure current flow, which could also be considered as contact resistance, in order to identify an additional mechanical property of the interaction. As illustrated in *Figure 5*, this other mechanical property is related to the area of contact between the sheets, determined by the amount of force applied to the sheets, and to the total area over which the force is applied; or a combination of these two properties. Thus, data relating to force and area may give useful information relating to the interaction, separate from the position at which the interaction takes place.

In some situations, such as when using a stylus or similar implement, the area of applied force remains substantially constant therefore a measurement of current will enable calculations to be made in terms of stylus pressure. Pressure sensitive styli are known but in known configurations the pressure detection is determined within the stylus itself, leading to the stylus being mechanically connected to operational equipment or requiring sophisticated wireless transmission within the stylus itself. The present embodiment allows stylus pressure to be determined using any non-sophisticated stylus, given that the pressure detection is made by the co-operating fabric detector, arranged to detect stylus position (with reference to

voltage) in combination with stylus pressure, with reference to current.

An alternative construction for the conducting fabric planes is illustrated in *Figure 6*. The detector includes a first conducting plane **601** and a second conducting plane **602**. In addition, woven into each of the conducting planes **601** and **602**, there are a plurality of non-conducting nodes **605** arranged to mutually interfere and thereby separate the two conducting planes. Between the nodes, the fabrics of the first and second planes may be brought into contact relatively easily such that the application of force, illustrated by arrow **611** would tend to cause a finite number of regions interspersed between nodes **605** to be brought into contact. Thus, for a particular region, contact either is taking place or is not taking place as illustrated by curve **621**.

With a number of such regions brought into contact, the overall level of current flow will tend to vary with the area of contact as illustrated by curve **631**. Thus, using a construction of the type shown in *Figure 6*, it is possible to obtain a more linear relationship, compared to that shown in *Figure 5*, in which the level of current flow gives a very good indication of the area of coverage as distinct from the level of force applied to the mechanical interaction.

Given a construction of the type shown in *Figure 6*, an indication of applied force or pressure may be obtained, in addition to an accurate determination of area, by providing an incremental switching operation. In the configuration shown in *Figure 7*, there is provided a first conducting plane **701** which interacts with a second conducting plane **702**. Furthermore, conducting plane **702** interacts with a third conducting plane **704**. Conducting plane **701** is separated from conducting plane **702** by non-conducting portions **705**. Similarly, plane **702** is separated from plane **704** by non-conducting portions **706**. More non-conducting portions **705** are provided than similar non-conducting portions **706**. Consequently, less force is required to produce electrical contact between planes **701** and **702** than is

required to produce an electrical contact between planes **702** and **704**. In this way, it is possible to provide an incremental measurement of force, given that a low force will only cause contact between plane **701** and plane **702** whereas a larger force will also provide electrical contact between plane **702** and **704**.

5 An alternative configuration is shown in *Figure 8* in which it is possible to obtain enhanced substantially continuous variations in current flow with respect to applied force. A first conducting plane **801** interacts with a second conducting plane **802**. The planes are woven in such a way as to produce  
10 very uneven surfaces such that, under light load, the level of interaction is relatively low. As load increases, as illustrated generally at **805**, a greater level of surface contact shown at **806** is created thereby increasing the level of current flow in a substantially continuous way. It should also be noted that this configuration does not include an insulating layer as such and that a level  
15 of current flow will always take place even under conditions of zero load. Alternatively, a very thin insulating layer could be provided, having a relatively low threshold, thereby resulting in a zero current flow when no load is applied.

As shown by curve **811**, the output current varies with respect to variations in applied force for a constant load area. Similarly, as shown by  
20 curve **821**, output current varies with respect to load area for a substantially constant applied force.

A composite configuration is shown in *Figure 9*, in which a detector **901**, substantially similar to that shown in *Figure 6*, is combined with a  
25 detector **902**, substantially similar to that shown in *Figure 9*. Detector **901** provides an accurate measurement of applied area and it is relatively unaffected by applied force. Detector **902**, as shown in *Figure 8*, provides an output which varies with respect to area and force. Thus, by processing the output of these two detectors in combination, it is possible to compensate the  
30 output from detector **902** in order to produce values representing force, such

that the two currents provide indications of both force and area.

The operation of the control circuit 121 is such as to apply a first voltage across diagonals 107 and 108 with a similar voltage being applied across diagonals 111 and 112. The nature of the voltage distribution is therefore asymmetric, but this does not result in difficulties provided that the area of contact between the two planes is relatively symmetric. However, should an asymmetric area of contact be made, as illustrated in *Figure 10*, differences will occur in terms of current measurements when considering calculations made in the two directions.

An asymmetric object 1001 is shown applied to the surface of a detector 1002. When a voltage is applied between contact 107 and 108, paths over which current may flow, illustrated generally at 1003 are relatively large and the object is perceived as having a large area or is perceived as applying a large force. In the opposite dimension, when a voltage is applied between 111 and 112, the regions over which current flow takes place illustrated generally at 1105, become relatively smaller therefore the object would be perceived as having a relatively smaller area or would be perceived as providing a relatively smaller force.

If the system is programmed to the effect that the object has a constant area and applies a constant force, these differences in terms of current flow may be processed in order to give an indication as to the orientation of the object. Thus, the system of the type illustrated in *Figure 10*, is used in combination with the detector of the type illustrated in *Figure 9* it is possible to make reference to the parameters of location in two-dimensions, force or pressure, the area of application and orientation.

In the preferred embodiment, electrical characteristics of voltage and current are measured. Alternatively, it would be possible to determine the resistance or the resistivity of the conducting sheets. Problems may be encountered when using alternating currents due to energy being radiated from the conducting sheets. However, in some situations it may be preferable

to use alternating currents, in which further electrical characteristics of the detector may be considered, such as capacitance, inductance and reactance etc.

5 The detector shown in *Figure 1*, constructed from conducting planes **102** and **103**, operates satisfactorily if the plane of the detector is maintained substantially flat. This does not create a problem in many applications where relatively flat operation is considered desirable. However, although constructed from fabric, thereby facilitating bending and folding operations, the reliability of the detector in terms of its electrical characteristics cannot be  
10 guaranteed if the detector planes are folded or distorted beyond modest operational conditions.

A detector is shown in *Figure 11*, constructed from fabric having electrically conductive elements to define at least two electrically conductive planes. The detector is configured to produce an electrical output in response  
15 to a mechanical interaction, as illustrated in *Figure 1*. At least one of the planes includes first portions and second portions in which the first portions have a higher resistance than said second portions and the first higher resistance portions are more flexible than the second portions. In this way, flexing occurs at the portions of high resistance, where contact between the  
20 planes has little effect, while the lower resistance portions, where contact does have a strong electrical effect, remain substantially rigid such that the flexing of the material does not occur over these portions of the detector.

Portions **1101** have a relatively high resistance compared to portions **1102**. Portions **1101** are not involved in terms of creating an electrical  
25 reaction in response to a mechanical interaction. The electrical responses are provided by the more rigid weave of portions **1102**. The purpose of portions **1101** is detailed in *Figure 11B*. A curvature has been applied to the detector but the configuration is such that normal operation is still possible. The flexing has occurred predominantly at portions **1101**. However, portions **1102** have  
30 remained straight thereby ensuring that they remain displaced from each

other, even when a curvature is present, such that the detector is still available for detecting the presence of a mechanical interaction.

The rigidity of portions **1102** may be enhanced as shown in *Figure 12A*. A first plane **1201** has rigid portions **1202** and flexible portions **1203**. A second plane **1204** has relatively rigid portions **1205** and relatively flexible portions **1206**. The relatively flexible portions **1206** physically contact against similar portions **1203** in the first plane **1201**. In order to ensure that there is no, or at least minimal electrical interaction at these points of contacts, the electrical resistance of the flexible portions **1203** and **1206** is relatively high. A partially insulating layer may be provided between the conducting layers, as shown in *Figure 1*. However, the flexible portions **1203** act as insulating separators therefore in this embodiment the provision of a separation layer is not essential. Furthermore, the rigidity of the interacting sections, in terms of the rigid portions **1202** and **1205**, has its rigidity further enhanced by the presence of relatively solid intermediate plates **1208**.

Flexing of the construction shown in *Figure 12A* is substantially similar to that provided by the embodiment shown in *Figure 11B*. The flexing of the embodiment shown in *Figure 12A* is detailed in *Figure 12B*. Flexing occurs at the position of the relatively flexible portions **1203** and **1206**. The rigidity of portions **1202** and **1205** is enhanced by the provision of more solid plates **1208**. Thus, the embodiment shown in *Figures 12A* and *12B* may have more strenuous flexing forces applied thereto such that mechanical interaction detection is maintained even under severe operating conditions.

The provision of the flexible portions effectively provide lines over the surface of the conducting planes where folding is permitted. Thus, complex curvatures may be obtained by a number of folds being effected at a plurality of these preferred foldable lines, thereby allowing complex shapes to be attained while maintaining the desired electrical characteristics.

An alternative embodiment is shown in *Figure 13* in which a first co-operating plane has flexible high resistive portions **1301** and rigid conducting



portions 1302. This plane co-operates with a second plane 1303 of substantially homogenous construction. Thus, sufficient flexing and insulation is provided by the non-conducting flexible portions 1301 of the lower co-operating plane 1304. The rigidity of conducting portions 1302 may be enhanced in a fashion substantially similar to that provided by *Figure 12A* as illustrated in *Figure 14*. The device includes an outer plane 1401 of substantially homogenous conducting construction. Below this, there is provided a second co-operating plane 1402 and the two planes may be separated by an insulating layer not shown in the example. The second plane or layer includes flexible non-conducting portions 1403 and more rigid conducting portions 1404, substantially similar to those shown in *Figure 13*. In addition, rigid plates 1405 are provided below each rigid portion 1404 thereby significantly enhancing the rigidity of these portions. Thus, the construction in *Figure 4* is capable of withstanding more aggressive working environments compared to the lighter construction shown in *Figure 13*.

In the construction shown in *Figures 13* and *14* the outer layers, 1303 and 1401 respectively, are fabricated in a substantially elastic fashion, thereby providing for a stretching or extension of this layer during flexing operations.

The detector shown in *Figure 1* is capable of accurately detecting the position of a mechanical interaction and as previously described, it is also possible to determine other characteristics of the mechanical interaction by modifying other electrical properties. A problem with the detector shown in *Figure 1* is that it experiences difficulties if more than one unconnected mechanical interaction takes place. If a first mechanical interaction were to take place and, simultaneously, a second mechanical interaction were to take place, displaced from the first, it would not be possible, using the configuration shown in *Figure 1*, to identify the presence of two mechanical interactions. A condition would be detected to the effect that a mechanical interaction is taking place but the system would tend to perceive this as a

single mechanical interaction having characteristics substantially similar to the average of the characteristics of the two independent interactions.

An alternative embodiment for overcoming problems of this type is shown in *Figure 15*. In *Figure 15*, a plurality of detectors **1501**, **1502**, **1503**, **1504**, **1505**, **1506** and **1507** have been connected together and each of these individual detectors has its own unique connectors **1511**, **1512**, **1513** and **1514**. In this way, each of the individual detectors may be connected to its own respective control circuit, such as circuit **121** shown in *Figure 1* or, in an alternative embodiment, a single control circuit of the type shown in *Figure 1* may be shared, using a switching arrangement, between all seven of the individual combined detectors. In this way, each individual detector, such as detector **1501**, provides the same level of accuracy as the detector shown in *Figure 1*. However, if two or more mechanical interactions take place on different detector sections, it is possible to detect this condition and provide appropriate output responses. However, it is only possible to detect a plurality of mechanical interactions if these interactions take place on different sections and it is not possible for the embodiment shown in *Figure 15* to detect a plurality of interactions if these interactions take place on the same section.

In the arrangement shown in *Figure 15*, the detectors have been arranged in strips such that there is enhanced definition in the direction of arrow **1521** but the definition in the direction of arrow **1522** has not changed.

In the detector shown in *Figure 1*, position detection is made possible using four electrical connection cables, a first two connected to opposing diagonal corners of the upper sheet and a further two connected to the alternative opposing diagonal corners of the lower sheet. An alternative configuration is shown in *Figure 16* in which electrical connectors **1601**, **1602**, **1603** and **1604** are connected to respective corners **1611**, **1612**, **1613** and **1614** of a lower plane conducting sheet

1621. An upper plane conducting sheet 1622 is connected to a single detecting cable 1631 connected at a position 1632 towards an edge of upper conducting sheet 1622. A disadvantage of the configuration shown in *Figure 16* is that five separate electrical connections are required whereas only four electrical connections are required in the configuration shown in *Figure 1*. However, in some circumstances, the configuration shown in *Figure 16* does have advantages over that shown in *Figure 1*.

The configuration shown in *Figure 16* may be used to effectively multiplex the operation of a detector so as to facilitate the detection of a plurality of mechanical interactions to a greater extent than the configuration shown in *Figure 15*. In particular, it facilitates detecting multiple mechanical interactions in both dimensions of the planar detector.

As shown in *Figure 17*, a lower planar sheet 1701 has connections 1702, 1703, 1704 and 1705 at each of its corners. Thus, sheet 1701 operates in a way which is substantially similar to the operation of sheet 1621 and all output voltages are generated within this sheet, either across diagonal 1702 to 1704 or across diagonal 1703 to 1705, thereby giving a two-dimensional co-ordinate within the area of the sheet.

An upper planar sheet 1721 is divided into a plurality of portions. In the example shown, eight portions 1731 to 1738 are provided. Thus, the mechanical action results in conducting planes of at least one of said regions being brought into electrical interaction with the lower plane 1701. Furthermore, if a mechanical interaction occurs at region 1731 and a second mechanical interaction occurs at region 1735 (for example) both of these mechanical interactions may be determined independently and an output to this effect may be generated by a processing system, such as system 131.

In order to achieve the space division multiplexing provided by regions 1731 to 1738, time division multiplexing of the electrical signals is performed in which, during each individual time slot, one individual region

1731 to 1738 is considered. This is achieved by each individual region 1731 to 1738 having its own respective electrical connector 1741 to 1748. These connectors are preferably incorporated in to the structure of the sheet.

5           Control circuitry for the configuration shown in *Figure 17* requires modification compared to that shown in *Figure 2*. In particular, each of the eight output control lines 1741 is supplied to its own respective buffering amplifier, similar to amplifiers 2223 and 2223 and the output from each of these eight amplifiers is applied to appropriate switching devices, allowing  
10           one of eight inputs to be selected using a plurality of switches substantially similar to switch 2221.

          A complete scanning cycle consists of applying a voltage between input terminals 1702 and 1704. An output is then considered from each individual output terminals 1741 to 1748. The voltages are then reversed  
15           such that a voltage is applied between output terminals 1705 and 1703. Each of the individual input terminals is then considered again so as to provide two-dimensional co-ordinates within each of the individual regions 1731 to 1748. As described with respect to *Figure 2*, both voltages and currents may be considered in order to provide additional mechanically  
20           related information, such as pressure related information etc.

## Claims

1. A detector constructed from fabric having electrically  
conductive elements and configured to produce electrical outputs in response  
5 to mechanical interactions, wherein

a detector is divided into a plurality of regions;

each of said regions includes a first conducting plane and a second  
conducting plane; and

a mechanical interaction results in conducting planes of at least one of  
10 said regions being brought closer together.

2. A detector according to claim 1, wherein at least one of said  
conducting planes is unique to a region and the co-operating conducting  
plane is shared with a plurality of regions.

15

3. A detector according to claim 2, wherein a single co-operating  
conducting plane is shared with all of said regions.

4. A detector according to any of claims 1 to 3, wherein signals  
20 are derived independently from a plurality of regions by a time division  
multiplexing operation.

5. A detector according to any of claims 1 to 4, wherein at least  
one of said planes includes first portions and second portions, said first  
25 portions have a higher resistance than said second portions and said first  
higher resistance portions are more flexible than said second portions.

6. The detector according to claim 5, wherein said higher  
resistance portions are configured as flexible portions to facilitate rotational  
30 movement about similar portions in a co-operating conductive plane.

7. A detector according to claim 5 or claim 6, wherein said second portions are further supported by solid portions.

5 8. A detector according to claim 7, wherein said solid portions are constructed from rubber, silicon or plastics.

9. A detector according to any of claims 1 to 8, wherein a potential is applied across at least one of said planes to determine the position of the  
10 mechanical interaction, and a second electrical property is determined to identify additional properties of said mechanical interactions.

10. A detector according to claim 9, configured to measure current or resistance as said second electrical property.

15 11. A detector according to claim 9 or claim 10, configured to determine applied force, applied pressure, area of contact or orientation of an object as the additional property of said mechanical interactions.

20 12. A method of constructing a detector from fabric having electrically conductive elements and configured to produce electrical outputs in response to mechanical interactions, comprising the steps of

dividing the detector into a plurality of regions;

25 providing a first conductive plane and a second conductive plane for each of said regions; and

bringing together conductive planes of at least one of said regions in a response to a mechanical interaction.

30 13. A method of constructing a detector according to claim 12, wherein at least one of said conducting planes is unique to a region and the

co-operating conducting plane is shared with a plurality of regions.

14. A method according to claim 13, wherein a single co-operating conducting plane is shared with all of said regions.

5

15. A method according to any of claims 12 to 14, wherein signals are derived independently from a plurality of regions by a time division multiplexing operation.

10

16. A method according to any of claims 12 to 15, wherein at least one of said planes includes first portions and second portions, said portions have a higher resistance than said second portions and said first higher resistance portions are more flexible than said second portions.

15

17. A method according to claim 16, wherein said higher resistance portions are configured as flexible portions to facilitate rotational movement about similar portions in a co-operating conductive plane.

20

18. A method according to claim 16 or claim 17, wherein said second portions are further supported by solid portions.

19. A method according to claim 18, wherein said solid portions are constructed from rubber, silicon or plastics.

25

20. A method according to any of claims 12 to 19, wherein a potential is applied across at least one of said planes to determine the position of the mechanical interaction, and a second electrical property is determined to identify additional properties of said mechanical interactions.

21. A detector constructed from fabric substantially as herein described with reference to *Figures 15, 16 and 17.*

22. A method of constructing a detector from fabric, substantially as  
5 herein described with reference to *Figures 15, 16 and 17.*





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Claims searched: All

Examiner: Mark A Pullen  
Date of search: 20 January 2000

**Patents Act 1977**  
**Search Report under Section 17**

**Databases searched:**

UK Patent Office collections, including GB, EP, WO & US patent specifications, in:

UK CI (Ed.R): G1N (NACH, NACNR, NAEPR, NAFD8, NAGB8, NAGBR, NAQB),  
H1N (NBH, NUJD)

Int CI (Ed.7): G01L 1/20, G06K 11/12, 11/16

Other: ONLINE : WPI, EPODOC, JAPIO

**Documents considered to be relevant:**

Category	Identity of document and relevant passage	Relevant to claims
X,Y	GB 1308575 (DATA APPLIANCE) see page 2 lines 17-89	X:1-3, 12-14 Y:4,15
Y	US 4963703 (PHILLIPS et al) see all Figures	4,15

X	Document indicating lack of novelty or inventive step	A	Document indicating technological background and/or state of the art
Y	Document indicating lack of inventive step if combined with one or more other documents of same category.	P	Document published on or after the declared priority date but before the filing date of this invention.
&	Member of the same patent family	E	Patent document published on or after, but with priority date earlier than, the filing date of this application.